

July 29, 2013

Mr. John Criste TERRA NOVA PLANNING & RESEARCH, INC. 42635 Melanie Place Palm Desert, CA 92211

Subject: Monterey Avenue Improvement Project Traffic Impact Analysis (Revised)

Dear Mr. Criste:

INTRODUCTION

Urban Crossroads, Inc. is pleased to provide this revised letter documenting our analysis of the proposed Monterey Avenue Improvement Project. The report has been revised based on input from the City of Rancho Mirage staff and now includes additional truck traffic volume data and Opening Year analysis. The Monterey Avenue Improvement Project proposes to widen Monterey Avenue to its ultimate width as a six (6) lane primary arterial roadway by constructing an additional southbound lane from south of Market Place Way to south of A Street. The project area is generally depicted on Exhibit A. This "missing link" widening will provide a continuous 3rd southbound lane from the I-10 Freeway to south of Country Club Drive. Exhibit A illustrates the location of the project area. Analysis of Existing, Opening Year (2014), and Long Range (2035) conditions has been conducted to evaluate the potential impact of the project on traffic operations within the affected area of Monterey Avenue corridor and identify improvements necessary to provide acceptable traffic operations.

The proposed widening of the Monterey Avenue is necessary to accommodate the growth in traffic that is contemplated as the adjacent Cities of Rancho Mirage and Palm Desert continue to experience ongoing growth in accordance with their respective General Plan Land Use Elements as reflected in regional projections of long term growth.

The Monterey Avenue widening project is consistent with the City of Rancho Mirage and City of Palm Desert General Plan Circulation Elements. Both Opening Year (2014) and Long Range (2035) with and without the project (Monterey Avenue roadway widening) conditions will be evaluated in this traffic analysis. The study objectives include (1) documentation of existing traffic conditions; (2) evaluation of traffic conditions for Opening Year (2014) conditions; and (3) evaluation of traffic conditions for Long Range (2035) conditions.

PROJECT DESCRIPTION

The project is proposed to widen Monterey Avenue to a consistent 6 (through) lane divided cross-section throughout the project area (and beyond). This "missing link" widening will provide a continuous 3rd southbound lane from the I-10 Freeway to south of Country Club Drive. The intent of the project is to limit improvements to the west side of Monterey Avenue (constructing a third travel lane, along with associated curb, gutter, and sidewalks).

STUDY AREA

Exhibit B illustrates the project location and traffic analysis study area. Monterey Avenue is a major subregional corridor that serves traffic traveling to and from the Interstate 10 (I-10) Freeway, which is located just north of Dinah Shore Drive. South of Highway 111, Monterey Avenue becomes State Route 74 (SR-74), providing access to the San Jacinto mountains, as well as access to other destinations in Riverside and San Diego Counties.

The study area includes the following intersection:

| ID | Intersection Location | Jurisdiction |
|----|------------------------------------|---------------------------------------|
| 1 | Monterey Avenue / Dick Kelly Drive | City of Rancho Mirage and Palm Desert |

TRAFFIC OPERATIONS ANALYSIS METHODOLOGIES

This section presents the methodologies for the analyses prepared in this assessment, which includes overall methodologies used to develop future traffic volume forecasts and explicit traffic operations analysis methodologies.

Overall Analysis Methodology

Existing conditions data has been collected / compiled explicitly for this work effort. Peak hour turning movement counts were collected for the study area intersection in November, 2012. Daily traffic volume data was compiled from available resources, specifically the Coachella Valley Association of Governments 2013 annual traffic census, or estimated based on the peak hour data.

The long range traffic volumes have been obtained from a combination of sources, including the Riverside Transportation Analysis Model (RIVTAM) and forecasts from the previously published report Monterey Commons Retail Development Traffic Impact Analysis (Revised), Urban Crossroads, Inc. 2008. The volumes contained in the Monterey Commons project traffic study report have been derived from the Coachella Valley SubArea Transportation Model Study CVSATM (Coachella Valley Subarea Applications



Traffic Model). The RIVTAM forecasts within the study area indicated somewhat less growth in through traffic compared to the volumes presented in the previously published Monterey Commons project traffic study report. However, the RIVTAM roadway network is not sufficiently detailed to show the traffic using the west leg of the intersection (Ginger Rogers Road) under 2035 conditions. Therefore, the previously published forecasts were used to determine forecast traffic movements to and from Ginger Rogers Road and Dick Kelly Drive, while the previously published through traffic volumes were adjusted based on review of the RIVTAM forecasts to ensure greater consistency with the forecasts being used for projects throughout the Coachella Valley (and Riverside County).

Opening Year (2014) traffic volumes were estimated based on straight line interpolation between the existing (2012) and Long Range (2035) traffic volumes. Since the Opening Year (2014) data is dependent on the Long Range (2035) data, the Opening Year volumes and analysis are generally presented subsequent to the Long Range (2035) volumes and analysis.

Level of Service

Traffic operations of roadway facilities are described using the term "Level of Service" (LOS). LOS is a qualitative description of traffic flow based on several factors such as speed, travel time, delay, and freedom to maneuver. Six levels are typically defined ranging from LOS "A", representing completely free-flow conditions, to LOS "F", representing breakdown in flow resulting in stop-and-go conditions. LOS "E" represents operations at or near capacity, an unstable level where vehicles are operating with the minimum spacing necessary to maintain uniform flow.

Intersection Capacity Analysis Methodology

Intersection capacity analyses are performed using the 2000 Highway Capacity Manual (HCM) methodology. The computer software program, Synchro, has been utilized to calculate the intersection delay values and resulting Levels of Service (LOS). Synchro is a traffic signal progression analysis software that is capable of performing intersection delay analyses using various methodologies, including the HCM method.

The HCM defines Level of Service (LOS) as a qualitative measure which describes operational conditions within a traffic stream, generally in terms of such factors as speed and travel time, freedom to maneuver, traffic interruptions, comfort and convenience, and safety. The criteria used to evaluate LOS conditions vary based on the type of roadway and whether the traffic flow is considered interrupted or uninterrupted.

The definitions of LOS for interrupted traffic flow (flow restrained by the existence of traffic signals and other traffic control devices) differ slightly depending on the type of traffic control. The LOS is typically dependent on the quality of traffic flow at the intersections along a roadway. The *Highway Capacity Manual* (HCM) (Transportation Research Board 2000) methodology expresses the LOS at an



intersection in terms of delay time for the various intersection approaches. The HCM uses different procedures depending on the type of intersection control.

The intersection LOS analysis in this report is based on the traffic volumes observed during the peak hour conditions using peak period traffic count data collected November 8, 2012 (Thursday). The following peak hours were selected for analysis:

- Weekday AM Peak Hour (peak hour between 7:00 AM and 9:00 AM)
- Weekday PM Peak Hour (peak hour between 4:00 PM and 6:00 PM)

For Signalized intersections, the City of Rancho Mirage and City of Palm Desert requires signalized intersection operations analysis based on the methodology described in Chapter 16 of the 2000 HCM. Intersection LOS operations are based on an intersection's average control delay. Control delay includes initial deceleration delay, queue move-up time, stopped delay, and final acceleration delay. For signalized intersections LOS is directly related to the average control delay per vehicle and is correlated to a LOS designation as described in Table 1.

Table 1 Signalized Intersection LOS Thresholds

| Level of | | Average Control |
|----------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------|
| Service | Description | Delay (Seconds) |
| А | Operations with very low delay occurring with favorable progression and/or short cycle length. | 0 to 10.00 |
| В | Operations with low delay occurring with good progression and/or short cycle lengths. | 10.01 to 20.00 |
| С | Operations with average delays resulting from fair progression and/or longer cycle lengths. Individual cycle failures begin to appear. | 20.01 to 35.00 |
| D | Operations with longer delays due to a combination of unfavorable progression, long cycle lengths, or high V/C ratios. Many vehicles stop and individual cycle failures are noticeable. | 35.01 to 55.00 |
| E | Operations with high delay values indicating poor progression, long cycle lengths, and high V/C ratios. Individual cycle failures are frequent occurrences. This is considered to be the limit of acceptable delay. | 55.01 to 80.00 |
| F | Operation with delays unacceptable to most drivers occurring due to over saturation, poor progression, or very long cycle lengths | 80.01 and up |

Source: HCM 2000, Chapter 16



The peak hour traffic volumes have been adjusted using a peak hour factor (PHF) to reflect peak 15 minute volumes. Common practice for LOS analysis is to use a peak 15-minute rate of flow. However, flow rates are typically expressed in vehicles per hour. The PHF is the relationship between the peak 15-minute flow rate and the full hourly volume (e.g. PHF = [Hourly Volume] / [4 x Peak 15-minute Flow Rate]). The use of a 15-minute PHF produces a more conservative analysis as compared to analyzing vehicles per hour. Existing PHFs have been used for Existing (2012) and Opening Year (2014) traffic conditions. Long Range (2035) conditions have been evaluated using a PHF of 1.0.

Intersection Queuing Analysis Methodology

Traffic signal progression analysis has been conducted to evaluate vehicular queuing and stacking length requirements by considering the signal timing and physical spacing of intersections. The progression results have been based on the output from the Synchro software program.

The Synchro software program calculates the 95th Percentile Queue based on the Average Queue plus a 1.65 standard deviation. The 95th Percentile Queue, which may not ever be observed, is simply based on statistical calculations. In many cases, the 95th Percentile Queue will not be experienced due to upstream metering. If the intersection is at or near capacity, the 50th Percentile Queue (or the Average Queue) represents the maximum queue likely to be experienced on a typical cycle.

Definition of Deficiency

The definition of an intersection deficiency has been obtained from City of Rancho Mirage and the City of Palm Desert policies. The City of Rancho Mirage requires peak hour intersection operation of LOS "D" or better. The City of Palm Desert General Plan Circulation Element states that peak hour intersection operation of LOS "C" or better is generally acceptable. However, as traffic volumes in the City increase, LOS "C" represents a standard that is progressively more difficult and costly to achieve in urban areas. For peak operating periods, LOS "D" and/or a maximum volume to capacity ratio of 0.90 is provisionally considered the generally acceptable service level. The City of Palm Desert's LOS "C" goal should only be exceeded where maximum feasible intersection improvements have been implemented.

EXISTING TRAFFIC CONDITIONS

Exhibit C identifies the existing roadway through lanes for the study area roadways and the intersection controls at existing intersection analysis location. As shown on Exhibit C, Monterey Avenue is a six (6) lane divided roadway north of Market Place Way, a five (5) lane divided roadway between Market Place Way and A Street (located south of Dick Kelly Drive), with three northbound through lanes and two southbound through lanes along this segment, and a six (6) lane divided roadway north of Gerald Ford Drive. The posted speed limit along Monterey Avenue within the study area is 55 miles per hour (mph).



Exhibit D illustrates the existing curb conditions along Monterey Avenue. As shown, the curb conditions along the west side of Monterey Avenue vary from paved sidewalks to unpaved / dirt conditions. The areas lacking sidewalks will be improved as part of the proposed project.

Existing Traffic Volumes

Existing traffic counts were collected to establish baseline conditions in the study area and are also used as an input to the traffic volume forecasting process. Data was collected during the most recent peak season. The peak hour data was collected in November of 2012 and provides the basis for the detailed operations analysis contained in this report. The daily traffic volume data was obtained from the Coachella Valley Association of Governments (CVAG) and was collected as part of the CVAG annual traffic census. Exhibit E illustrates the existing average daily traffic (ADT) and AM/PM peak hour intersection traffic volumes for the study area. The existing ADT volumes presented on Exhibit E are based upon the CVAG 2013 Traffic Census Report and/or the peak hour turning movement traffic data collected by Urban Crossroads, Inc. using the following formula for each intersection leg:

[AM + PM Peak Hour Volume]/(0.061 + 0.078) = Daily Leg Volume

In the above formula, the constants of 6.10% and 7.80% are calculated AM and PM Peak Hour to ADT ratios based on the actual peak hour collected and daily traffic count data from CVAG. Both AM and PM peak hour volumes are included in the calculation to ensure that traffic generators such as schools that are primarily active during the AM peak hour are accurately reflected in the daily traffic estimates. Attachment "A" contains the traffic count data and peak hour to daily traffic relationship calculations.

The AM peak hour traffic volumes were determined by counting the two hour period between 7:00 to 9:00 in the morning. Similarly, the PM peak hour traffic volumes were identified by counting the two hour period from 4:00 to 6:00 in the evening. The count includes the vehicle classification as shown below:

- passenger cars (1 PCE)
- 2 axle trucks/buses/recreational vehicles (1.5 PCE)
- 3 axle trucks (2 PCE)
- 4 or more axle trucks (3 PCE)

The traffic count data has been reviewed and indicates that the truck traffic percentages remain fairly constant between the AM and PM peak periods, with trucks comprising between 2 and 4% of the overall traffic in the study area. The daily truck percentages and volumes have been calculated using the slightly higher / more conservative AM peak period data (approximately 4% trucks). The AM peak period data indicates that large 2-axle vehicles (trucks, buses, and recreational vehicles) comprise 2% of the overall traffic, while 3 axle and 4+ axle trucks each constitute 1% of the overall traffic in the study area. The



overall existing count volumes illustrated on the exhibits and used for the analysis for the study are calculated passenger car equivalent (PCE) volumes. The PCE factor for each classification is shown on the list above. Explicit existing conditions peak hour factors have been calculated using the data collected for this effort as well.

As indicated on Exhibit E, existing daily traffic volumes on Monterey Avenue range from 29,900 to 32,500 vehicles per day (VPD). The daily traffic volume on Dick Kelly Drive is approximately 3,800 VPD. Exhibit E also presents the existing truck volume and percentage of the total traffic.

For the peak hour traffic volumes, the general trend is higher southbound volumes on Monterey Avenue in the morning peak hour, mirrored by a higher northbound volume in the evening peak hour of traffic.

General Plan Circulation Network

Both the City of Rancho Mirage and the City of Palm Desert General Plan Circulation Element planned roadway systems are directly applicable within the study area. In addition the overall County of Riverside planned roadway system addresses the planned roadway system within the study area.

Exhibits F and G depict the General Plan Circulation Element roadway designations and planned cross-sections, respectively, for the City of Rancho Mirage. Per the City of Rancho Mirage General Plan Circulation Element, Monterey Avenue is planned as a 6-lane divided Major Arterial within the study area, with a 106 foot curb to curb cross-section in an overall 120 foot right-of-way. The City of Rancho Mirage General Plan Circulation Element does not include a designation for the extension of Dick Kelly Drive (identified as Ginger Rogers Road in the previously published traffic study report for the Monterey Commons project).

Exhibits H and I present the General Plan Circulation Element roadway designations and planned cross-sections, respectively, for the City of Palm Desert. The City of Palm Desert identifies Monterey Avenue as an Arterial Street throughout the study area. This designation again provides for a basic 6-lane divided cross-section, with a 102 foot curb to curb cross-section in an overall 150 wide right of way. The curb to curb width is similar to the City of Rancho Mirage width (4 feet difference total or 2 feet on each side of the roadway). The City of Palm Desert cross-section includes a substantially larger parkway area adjacent to the roadway proper.

Dick Kelly Drive is also shown on the City of Palm Desert General Plan Circulation Element, which identifies Dick Kelly Drive as a Secondary Street. The Secondary Street designation provides for a 60 feet curb to curb width within an overall right of way of 108 feet. The curb to curb width can accommodate two through lanes in each direction, with width for a left turn lane at intersections.



The County of Riverside General Plan represents the overall plan for Riverside County, including both unincorporated areas and incorporated local jurisdictions such as the Cities of Rancho Mirage and Palm Desert. The countywide plan has most recently been updated in the context of the Riverside County Integrated Project (RCIP). The purpose of the RCIP is to integrate the processes of planning land use, transportation improvements and preserving habitat for endangered species. A primary objective of the RCIP is to accommodate projected population growth within Riverside County by focusing development within areas that will be readily accessible, will provide a good quality of life for future residents, and will minimize environmental and community impacts, including impacts to sensitive habitats and endangered species.

The most current RCIP network is depicted on Exhibit J and the RCIP cross-sections are illustrated on Exhibit K. Monterey Avenue is designated as an Urban Arterial from Dinah Shore Drive to Gerald Ford Drive. An Urban Arterial features a 110 foot curb to curb cross-section within an overall right of way of 152 feet and provides a 6-lane divided roadway. This is slightly wider than the City standards, however the number of through travel lanes (6 through lanes) is consistent for all three agencies.

The City of Rancho Mirage and the City of Palm Desert designations for Monterey Avenue differ in terms of minor details, but provide for the same basic roadway cross-section of a 6-lane divided facility. The overall County of Riverside RCIP plan provides for a substantially narrower cross-section south of Gerald Ford Drive. The narrower cross-section of only 86 feet curb to curb (compared to the 100 foot plus cross-sections identified by both the City of Rancho Mirage and the City of Palm Desert) can serve as a 6-lane divided section, but lane widths are standard at best and little opportunity for additional turn lanes is available at intersections. It is therefore recommended that the City of Rancho Mirage and the City of Palm Desert coordinate with the County of Riverside to ensure that the County plans be updated to reflect an Urban Arterial, which is more consistent with the City designations.

EXISTING CONDITIONS TRAFFIC OPERATIONS ANALYSIS

Intersection Analysis

The Intersection traffic operations analysis results are summarized in Table 2 for existing traffic conditions, based on the existing intersection lane configuration. Intersection delay analysis calculation worksheets for existing traffic conditions are included in Attachment "B". The study area intersection is currently operating at an acceptable level of service (Level of Service "B" or better).

Queuing Analysis

Table 3 summarizes the estimated 50th and 95th percentile (%) queues, respectively, under existing conditions for the AM and PM peak hours of traffic on the roadway system. The 50th % queue length represents the average queue expected throughout the peak hour, while the 95th % queue length



represents a peak or desirable design queue length that would be expected 5% of the time. The queuing analysis worksheets are included in Attachment "C". As shown on Table 3, adequate storage is provided to accommodate vehicle queues under existing traffic conditions.

LONG RANGE (2035) CONDITIONS TRAFFIC VOLUMES

The long range traffic volumes have been obtained from a combination of sources, including the Riverside Transportation Analysis Model (RIVTAM) and forecasts from the previously published report Monterey Commons Retail Development Traffic Impact Analysis (Revised), Urban Crossroads, Inc. 2008. The volumes contained in the Monterey Commons project traffic study report have been derived from the Coachella Valley SubArea Transportation Model Study CVSATM (Coachella Valley Subarea Applications Traffic Model). The RIVTAM forecasts within the study area indicated somewhat less growth in through traffic compared to the volumes presented in the previously published Monterey Commons project traffic study report. However, the RIVTAM roadway network is not sufficiently detailed to show the traffic using the west leg of the intersection (Ginger Rogers Road) under 2035 conditions. Therefore, the previously published forecasts were generally used to determine forecast traffic movements to and from Ginger Rogers Road and Dick Kelly Drive, while the previously published through traffic volumes were adjusted based on review of the RIVTAM forecasts to ensure consistency with the forecasts being used for projects throughout the Coachella Valley (and Riverside County).

The initial model output data has been refined based on the actual traffic counts and other recently prepared traffic volume forecasts available for the study area. The peak hour directional roadway segment volume forecasts have been determined based on the procedures and guidelines of the National Cooperative Highway Research Program Circular 255 (NCHRP-255). The specific approach is based on the City of Rancho Mirage traffic model Long Range (2035) peak hour volumes development procedure. The model output of peak hour intersection approach/departure data is a necessary input to this approach. The existing traffic volumes serve as the starting point for the refinement process. The final Long Range (2035) traffic volumes have also been checked against previously published interim year forecasts to ensure that no negative growth compared to published interim year forecasts occurs. Attachment "D" includes the growth reasonableness review worksheets documenting the traffic growth for each individual movement and each intersection leg inbound and outbound volumes for peak hour and daily conditions.

Exhibit L illustrates the Long Range (2035) average daily traffic (ADT) and AM/PM peak hour intersection traffic volumes for the study area. Projected truck traffic percentages and volumes are also presented on Exhibit L. Substantial increases in traffic are anticipated throughout the study area. Consistent with the previously published report for the Monterey Commons project, an additional (west) leg of the intersection is assumed to be built in conjunction with adjacent development. Growth in traffic on



Monterey Avenue ranges between 64% and 78% in the AM / PM peak hours, with even higher growth anticipated for the side street traffic. The higher side street growth is reasonable, given the amount of vacant land adjacent to Dick Kelly Drive and future Ginger Rogers Road.

LONG RANGE (2035) TRAFFIC OPERATIONS ANALYSIS

Intersection Analysis

The intersection traffic operations analysis results are summarized in Table 4 for Long Range (2035) without project widening and with project widening traffic conditions.

For Long Range (2035) without widening conditions, the study area intersection is anticipated to operate at an unacceptable level of service (LOS "E") during the PM peak hour. Intersection delay analysis calculation worksheets are included in Attachment "E" for Long Range (2035) without widening conditions. The west leg of the intersection (eastbound approach and westbound departure lanes), along with a southbound right turn lane, and any necessary left turn lanes on Monterey Avenue (northbound left and southbound left) will be further analyzed and built in conjunction with development on the currently vacant land west of Monterey Avenue in the vicinity of Dick Kelly Drive. These improvements are not a part of the currently proposed project and are expected to be mitigated and constructed by the future developer when and if development occurs on the adjacent property.

For Long Range (2035) with project (Monterey Avenue widening) conditions, addition of the 3rd southbound lane will improve the PM peak hour level of service from LOS "E" to LOS "D", decreasing the PM peak hour delay by 9 seconds per vehicle. Intersection delay analysis calculation worksheets are included in Attachment "F" for Long Range (2035) with widening conditions.

Queuing Analysis

For Long Range (2035) Without Widening conditions, the estimated 50th and 95th percentile (%) queues, respectively, for the AM and PM peak hours of traffic on the roadway system are summarized in Table 5. The queuing analysis worksheets are included in Attachment "G".

As shown on Table 5, no 50th percentile queuing issue is anticipated. This indicates that no queue storage issue will be observed at least half the time. However, review of the 95th percentile queuing calculations in Table 5 suggests that occasional 95th percentile queuing issues would occur at the intersection of Monterey Avenue at Dick Kelly Drive under Long Range (2035) Without Widening



conditions. Potential queuing issues occur during the PM peak hour of traffic include the following turning movements:

Monterey Avenue / Dick Kelly Drive

- Northbound Left (95th Percentile)
- Southbound Left (95th Percentile)

The identified queuing issues will only occur if development of the vacant land in the vicinity of the subject intersection takes place. Any need to reconstruct the center median would be evaluated by the future developer in conjunction with such future development, and appropriate mitigation of project impacts would occur at the time of development.

For Long Range (2035) With Project (Monterey Avenue widening) conditions, the estimated 50th and 95th percentile (%) queues, respectively, for the AM and PM peak hours of traffic on the roadway system are summarized in Table 6. The queuing analysis worksheets are included in Attachment "H". As shown on Table 6, any occasional queuing issues would be reduced for Long Range (2035) With Widening conditions as a result of the proposed project (e.g., the proposed project will reduce any occasional queue storage issues at the study area intersection). The identified queuing issues will only occur if development of the vacant land in the vicinity of the subject takes place. Any need to reconstruct the center median would be evaluated by the future developer in conjunction with such future development, and appropriate mitigation of project impacts would occur at the time of development.

OPENING YEAR (2014) CONDITIONS TRAFFIC VOLUMES

The Opening Year (2014) traffic volumes have been developed using straight line interpolation between the existing (2012) conditions volumes and the Long Range (2035) traffic volumes. As no active development is occurring on the west side of Monterey Avenue, only existing movements are included for Opening Year (2014) conditions. Exhibit M illustrates the Opening Year (2014) average daily traffic (ADT) and AM/PM peak hour intersection traffic volumes for the study area. Projected truck traffic percentages and volumes are also presented on Exhibit M.

OPENING YEAR (2014) TRAFFIC OPERATIONS ANALYSIS

Intersection Analysis

The intersection traffic operations analysis results are summarized in Table 4 for Opening Year (2014) without project widening and with project widening traffic conditions. For both Opening Year (2014) without and with widening conditions, the study area intersection is anticipated to operate at acceptable



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levels of service. Intersection delay analysis calculation worksheets are included in Attachment "H" for Opening Year (2014) without widening conditions. The Opening Year (2014) with widening conditions operations analysis worksheets are included in Attachment "I"

RECOMMENDATIONS / CLOSING

Based on the analysis and findings presented in the previous sections of this report, the following recommendations have been developed:

 Monterey Avenue within the project limits should be constructed as a six lane divided roadway by constructing a third southbound through lane.

 Any additional intersection improvements will only be required in conjunction with future development of vacant land in the vicinity of the proposed project. Any improvements needed to serve this future development will be evaluated by the developer and constructed as appropriate mitigation at such time as nearby development occurs.

Urban Crossroads, Inc. is pleased to provide this traffic analysis letter report for your use. If you have any questions, please contact us at (949) 660-1994.

Respectfully submitted,

URBAN CROSSROADS, INC.

Carleton Waters, P. E.

Principal

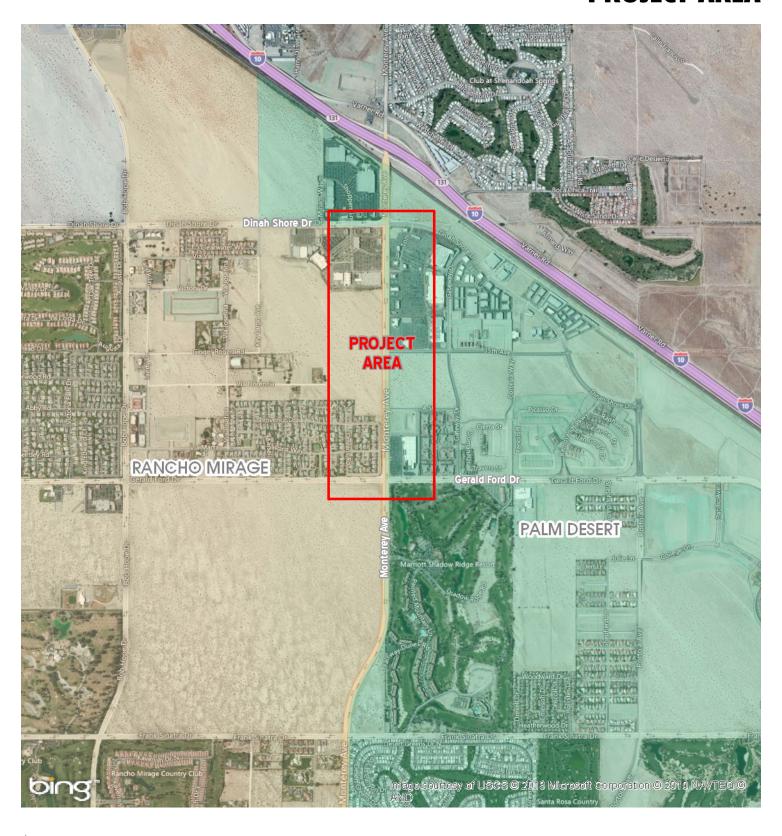
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Attachments



PROJECT AREA







LOCATION MAP



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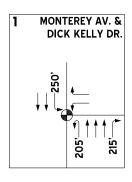






EXISTING NUMBER OF THROUGH LANES AND INTERSECTION CONTROLS





LEGEND:



- TRAFFIC SIGNAL
- = NUMBER OF LANES
- D DIVIDED

250' - POCKET LENGTH





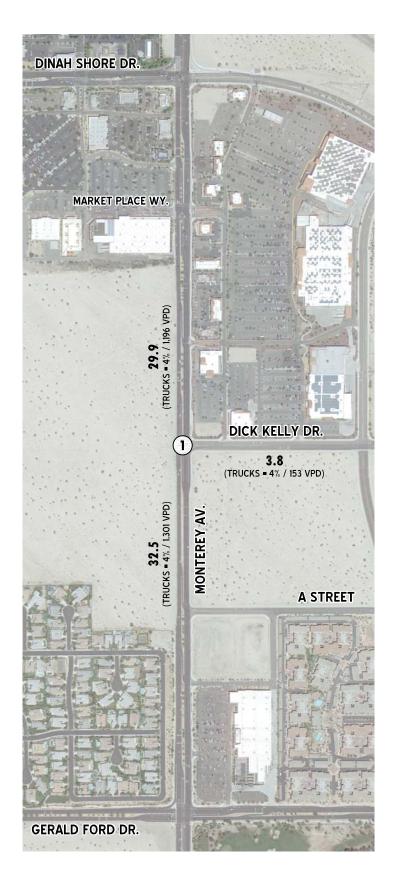
EXISTING MONTEREY AVENUE CURB CONDITIONS

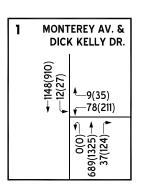






EXISTING (2012) TRAFFIC VOLUMES





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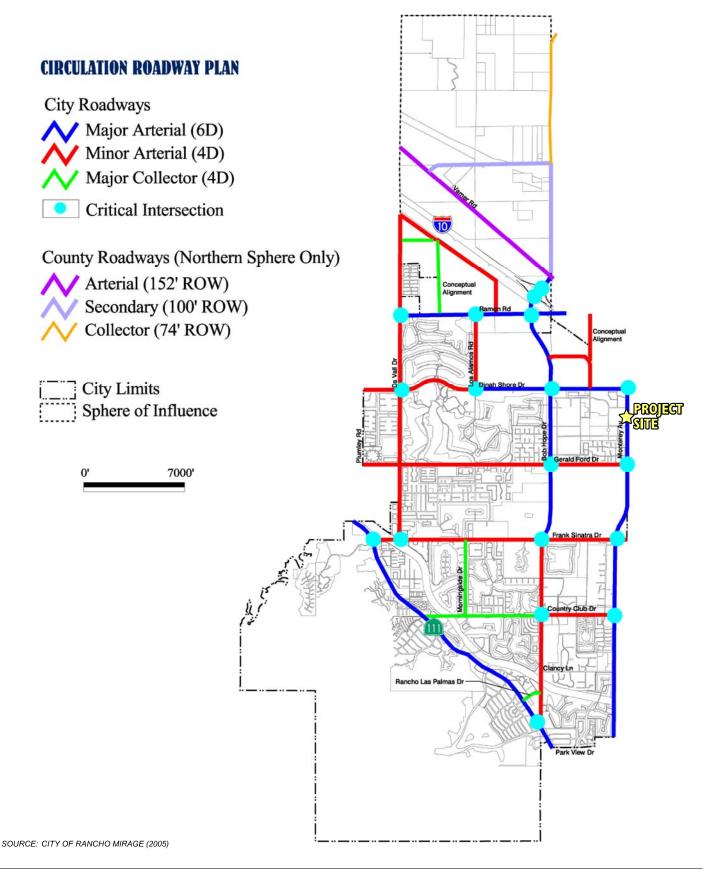
10.0 • VEHICLES PER DAY (1000'S)

10(10) - AM(PM) PEAK HOUR VOLUMES

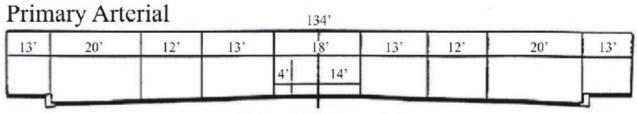




CITY OF RANCHO MIRAGE GENERAL PLAN CIRCULATION ELEMENT



CITY OF RANCHO MIRAGE GENERAL PLAN ROADWAY CROSS-SECTIONS



(Six Lanes divided, no parking)

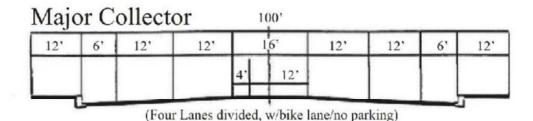
| Majo | or Arte | erial* | | 1 | 20' | | | | |
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| 7' | 20' | 12' | 13' | | 16' | 13' | 12' | 20' | 7' |
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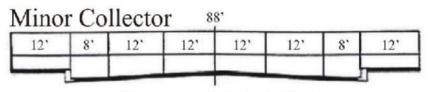
(Six Lanes divided, no parking)

*Highway 111 has special design geometrics. See Rancho Mirage Highway 111 Alignment Study, 1996.

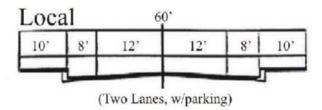
| 6' | 12' |
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| | |

(Four Lanes divided, w/bike lane/no parking)





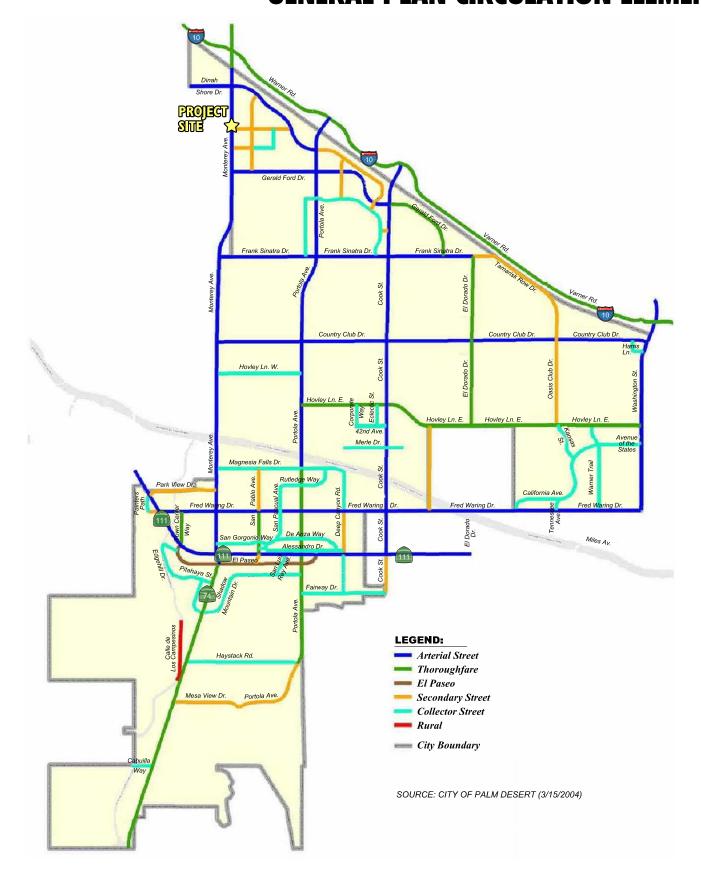
(Four Lanes undivided, w/parking)



SOURCE: CITY OF RANCHO MIRAGE (2005)



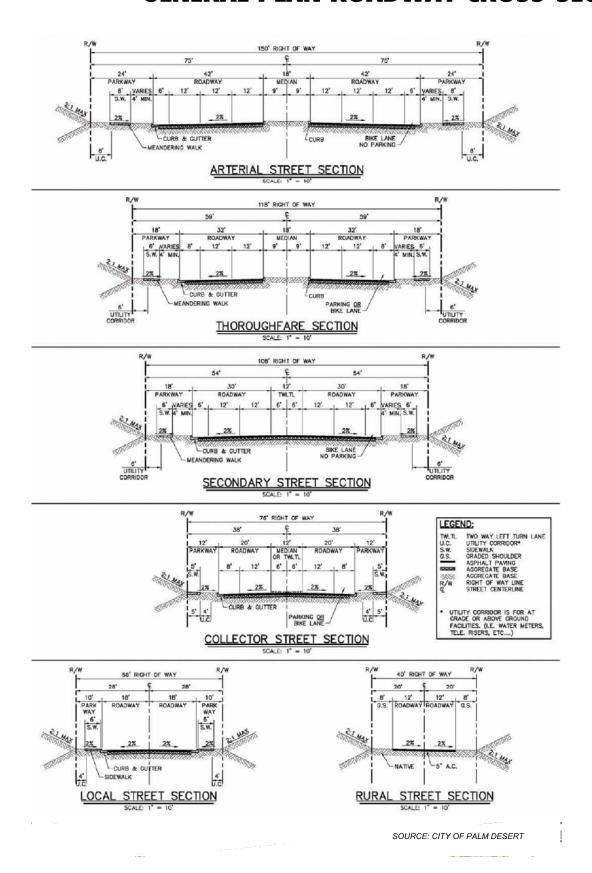
CITY OF PALM DESERT GENERAL PLAN CIRCULATION ELEMENT





EXHIBIT

CITY OF PALM DESERT GENERAL PLAN ROADWAY CROSS-SECTIONS



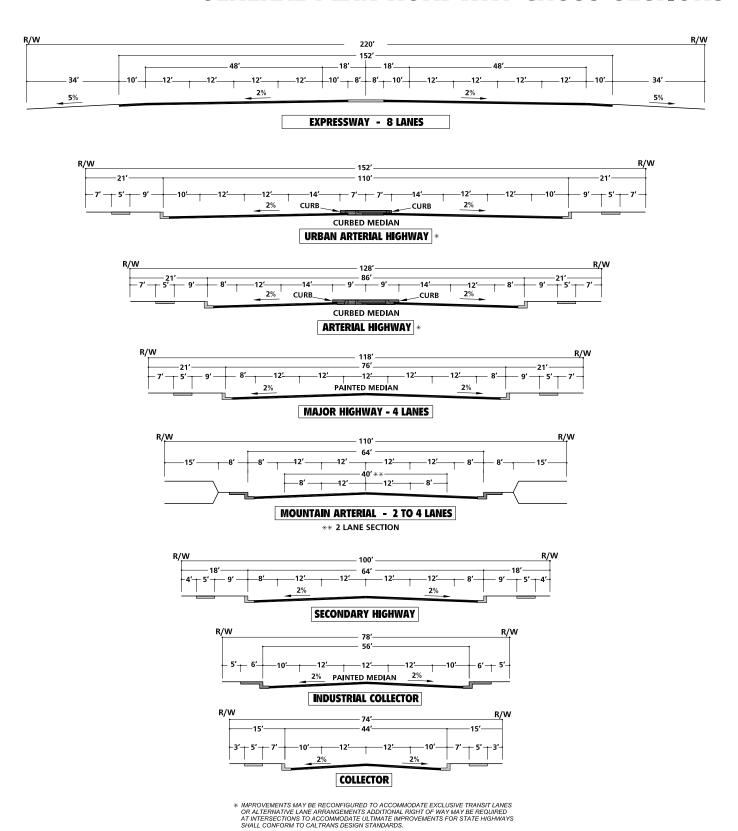


RIVERSIDE COUNTY GENERAL PLAN CIRCULATION ELEMENT





RIVERSIDE COUNTY GENERAL PLAN ROADWAY CROSS-SECTIONS

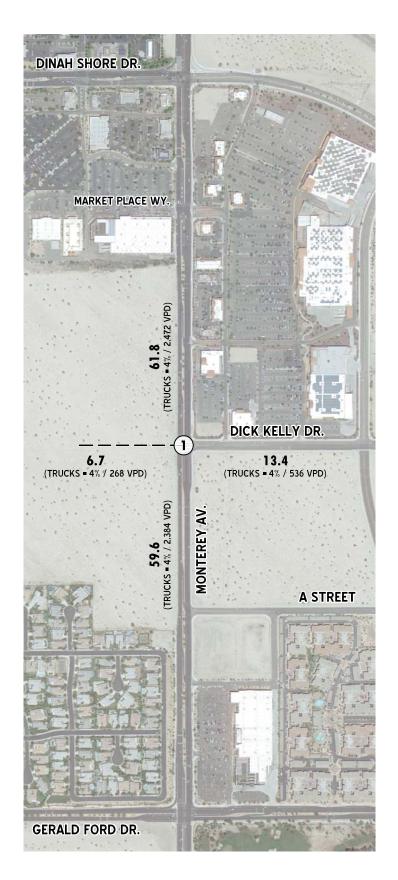


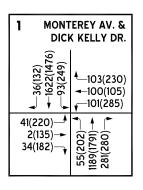
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SOURCE: COUNTY OF RIVERSIDE



LONG RANGE (2035) TRAFFIC VOLUMES





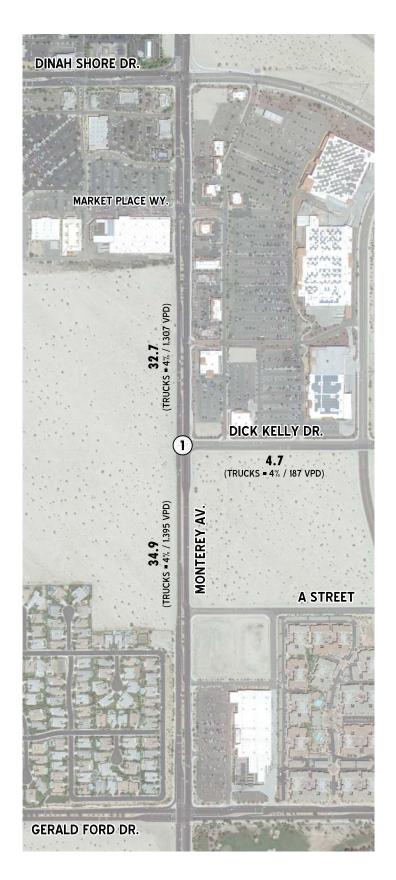
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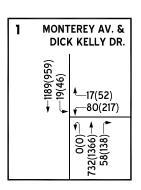
10.0 • VEHICLES PER DAY (1000'S) 10(10) • AM(PM) PEAK HOUR VOLUMES





OPENING YEAR (2014) TRAFFIC VOLUMES





LEGEND:

10.0 - VEHICLES PER DAY (1000'S)

10(10) - AM(PM) PEAK HOUR VOLUMES





Table 2
Intersection Analysis for Existing (2012) Conditions

| | | | | Intersection Approach Lanes ¹ | | | | | | | Del | av² | Lev | el of | | | | |
|---|-------------------------------|----------------------|------------|------------------------------------------|---|-----|-------------------|---|---|-----------|-----|-----|-----------|-------|-----|---------|----|------|
| | | Traffic | Northbound | | | Sou | Southbound Eastbo | | | Eastbound | | | Westbound | | | (secs.) | | vice |
| # | Intersection | Control ³ | L | Т | R | L | Т | R | L | Т | R | L | Т | R | АМ | PM | AM | PM |
| 1 | Monterey Av. / Dick Kelly Dr. | TS | 1 | 3 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 5.6 | 12.3 | Α | В |

- When a right turn is designated, the lane can either be striped or unstriped. To function as a right turn lane there must be sufficient width for right turning vehicles to travel outside the through lanes.
 - L = Left; T = Through; R = Right
- Per the 2000 Highway Capacity Manual, overall average intersection delay and level of service are shown for intersections with a traffic signal or all way stop control. For intersections with cross street stop control, the delay and level of service for the worst individual movement (or movements sharing a single lane) are shown.
- 3 TS = Traffic Signal



Table 3 Queuing Analysis for Existing (2012) Conditions

| | | | | 50th Per | centile | | | 95th Per | centile | |
|--------------------------------------|----------|---------------------|----|-------------------------------------|---------|-------------------------|---------------|---------------------------|-----------------------------|------|
| | Turning | Existing Storage | | Queue Length ² (feet) | | eue sue ³ | Queue (fee | Length ² t) | Queue Issue ³ | |
| Intersection | Movement | Length ¹ | AM | PM | AM | PM | AM | PM | AM | PM |
| Monterey Avenue | | | | | | | | | | |
| Dick Kelly Drive | NBU-Turn | 205 | 0 | 0 | O.K. | O.K. | 0 | 0 | O.K. | O.K. |
| | NBT | >1,000 | 28 | 150 | O.K. | O.K. | 74 | 175 | O.K. | O.K. |
| | NBR | 215 | 0 | 0 | O.K. | O.K. | 9 | 18 | O.K. | O.K. |
| | SBL | 250 | 10 | 22 | O.K. | O.K. | 31 | 52 | O.K. | O.K. |
| | SBT | >1,000 | 90 | 103 | O.K. | O.K. | 145 | 113 | O.K. | O.K. |

¹ Storage length (for turning movements) or internal link distance (for through movements).

² Queue Length is based on the (95th Percentile) queue length.

³ Storage length is O.K. if the queuing length is less than or equal to the existing storage length.

⁴ 95th percentile volumes exceed capacity. Queue may be longer

Table 4
Intersection Analysis for Long Range (2035) Conditions

| ſ | | | | | Intersection Approach Lanes ¹ | | | | | | | De | lay ² | Lev | el of | | | | |
|---|---|-----------------------------------------|----------------------|-----|------------------------------------------|---|---|----------|---|----------|----------|----------|------------------|-----|-------|------|------|----|----|
| | | | Traffic | Nor | orthbound Southbound Eastbound Westbound | | | | | | | Service | | | | | | | |
| | # | Intersection | Control ³ | L | Т | R | L | Т | R | L | Т | R | L | Т | R | АМ | PM | AM | РМ |
| | 1 | Monterey Av. / Dick Kelly Dr. | | | | | | | | | | | | | | | | | |
| | | - Without Project Widening ⁴ | TS | 1 | 3 | 1 | 1 | 2 | d | <u>1</u> | <u>1</u> | <u>1</u> | 1 | 1 | 0 | 22.6 | 59.0 | С | Е |
| | | - With Project Widening ⁵ | TS | 1 | 3 | 1 | 1 | <u>3</u> | 0 | <u>1</u> | <u>1</u> | <u>1</u> | 1 | 1 | 0 | 20.3 | 50.0 | С | D |

- ¹ When a right turn is designated, the lane can either be striped or unstriped. To function as a right turn lane there must be sufficient width for right turning vehicles to travel outside the through lanes.
 - L = Left; T = Through; R = Right; d = Defacto; $\underline{1}$ = Improvement
- ² Per the 2000 Highway Capacity Manual, overall average intersection delay and level of service are shown for intersections with a traffic signal. The study area intersection have been analyzed using the Synchro 8.0 software.
- 3 TS = Traffic Signal
- Monterey Avenue and Dick Kelly Drive is anticipated to be constructed as a 4-leg intersection based on the Monterey Commons traffic study (Urban Crossroads, 3/2008).
- ⁵ With Project widening. Provide a 3rd southbound through lane.
- * BOLD = LOS does not meet the applicable jurisdictional requirements (i.e., unacceptable LOS).



Table 5 Queuing Analysis for Long Range (2035) Without Widening Conditions

| | | Recommended | | | 50th Per | centile | | , | 95th Per | centile | |
|--------------------------------------|----------|-------------------------------------------|---------------------|---------------|----------------------------|---------|-------------------------|------------------|----------------------------|---------|------------------|
| | Turning | Storage Length ¹ (ft) per lane | Existing Storage | Queue (fee | Length ² et) | | eue sue ³ | Queue (fee | Length ² et) | | eue ue³ |
| Intersection | Movement | (95th Percentile) | Length | AM | PM | AM | PM | AM | PM | AM | PM |
| Monterey Avenue | | | | | | | | | | | |
| Dick Kelly Drive | NBL | 350 | 205 | 41 | 192 4 | O.K. | O.K. | 84 | 345 ⁵ | O.K. | YES ⁶ |
| | NBT | >1,000 | >1,000 | 183 | 427 | O.K. | O.K. | 272 | 600 ⁵ | O.K. | O.K. |
| | NBR | 215 | 215 | 0 | 39 | O.K. | O.K. | 47 | 115 | O.K. | O.K. |
| | SBL | 400 | 250 | 69 | 232 4 | O.K. | O.K. | 124 | 398 ⁵ | O.K. | YES ⁶ |
| | SBT | >1,000 | >1,000 | 471 | 533 4 | O.K. | O.K. | 770 ⁵ | 798 ⁵ | O.K. | O.K. |

¹ Recommended storage length (for turning movements) or internal link distance (for through movements) if queue length exceeds existing storage.



² Queue Length is based on the (95th Percentile) queue length.

³ Storage length is O.K. if the queuing length is less than or equal to the existing storage length.

⁴ Volume exceeds capacity, queue is theoretically infinite.

⁵ 95th percentile volumes exceed capacity. Queue may be longer

⁶ Provide minimum recommended storage length to address the potential queuing issue.

Table 6 Queuing Analysis for Long Range (2035) With Widening Conditions

| | | Recommended | | | 50th Per | centile | | | 95th Per | centile | |
|--------------------------------------|----------|-------------------------------------------|---------------------|---------------|----------------------------|---------|-------------------------|---------------|----------------------------|---------|------------------|
| | Turning | Storage Length ¹ (ft) per lane | Existing Storage | Queue (fee | Length ² et) | | eue sue ³ | Queue (fee | Length ² et) | | eue ue³ |
| Intersection | Movement | (95th Percentile) | Length | AM | PM | AM | PM | AM | PM | AM | PM |
| Monterey Avenue | | | | | | | | | | | |
| Dick Kelly Drive | NBL | 325 | 205 | 41 | 158 | O.K. | O.K. | 82 | 309 ⁵ | O.K. | YES ⁶ |
| | NBT | >1,000 | >1,000 | 175 | 441 | O.K. | O.K. | 272 | 626 ⁵ | O.K. | O.K. |
| | NBR | 215 | 215 | 0 | 44 | O.K. | O.K. | 47 | 124 | O.K. | O.K. |
| | SBL | 400 | 250 | 71 | 220 4 | O.K. | O.K. | 123 | 386 ⁵ | O.K. | YES ⁶ |
| | SBT | >1,000 | >1,000 | 270 | 368 | O.K. | O.K. | 412 | 489 | O.K. | O.K. |

¹ Recommended storage length (for turning movements) or internal link distance (for through movements) if queue length exceeds existing storage.



² Queue Length is based on the (95th Percentile) queue length.

³ Storage length is O.K. if the queuing length is less than or equal to the existing storage length.

⁴ Volume exceeds capacity, queue is theoretically infinite.

⁵ 95th percentile volumes exceed capacity. Queue may be longer

⁶ Provide minimum recommended storage length to address the potential queuing issue.

Table 7
Intersection Analysis for Opening Year (2014) Conditions

| | | | | Intersection Approach Lanes ¹ | | | | | | | | De | lay ² | Lev | el of | | | |
|---|-----------------------------------------|----------------------|-----|-------------------------------------------|---|---|----------|---|---------|---|---------|----|------------------|-----|-------|------|----|----|
| | | Traffic | Nor | Iorthbound Southbound Eastbound Westbound | | | | | (secs.) | | Service | | | | | | | |
| # | Intersection | Control ³ | L | Т | R | L | Т | R | L | Т | R | L | Т | R | АМ | PM | AM | PM |
| 1 | Monterey Av. / Dick Kelly Dr. | | | | | | | | | | | | | | | | | |
| | - Without Project Widening ⁴ | TS | 1 | 3 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 6.1 | 13.8 | Α | В |
| | - With Project Widening ⁵ | TS | 1 | 3 | 1 | 1 | <u>3</u> | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 5.7 | 13.6 | Α | В |

- ¹ When a right turn is designated, the lane can either be striped or unstriped. To function as a right turn lane there must be sufficient width for right turning vehicles to travel outside the through lanes.
 - L = Left; T = Through; R = Right; $d = Defacto; \underline{1} = Improvement$
- ² Per the 2000 Highway Capacity Manual, overall average intersection delay and level of service are shown for intersections with a traffic signal. The study area intersection have been analyzed using the Synchro 8.0 software.
- 3 TS = Traffic Signal
- ⁴ Monterey Avenue and Dick Kelly Drive is anticipated to be constructed as a 4-leg intersection based on the Monterey Commons traffic study (Urban Crossroads, 3/2008).
- ⁵ With Project widening. Provide a 3rd southbound through lane.



ATTACHMENT A

Traffic Count Data

Counts Unlimited, Inc. PO Box 1178 Corona, CA 92878 (951) 268-6268

City of Rancho Mirage N/S: Monterey Avenue E/W: Dick Kelly Drive Weather: Sunny

File Name: RNMMODKAM Site Code: 00000031

Start Date : 11/8/2012 Page No : 1

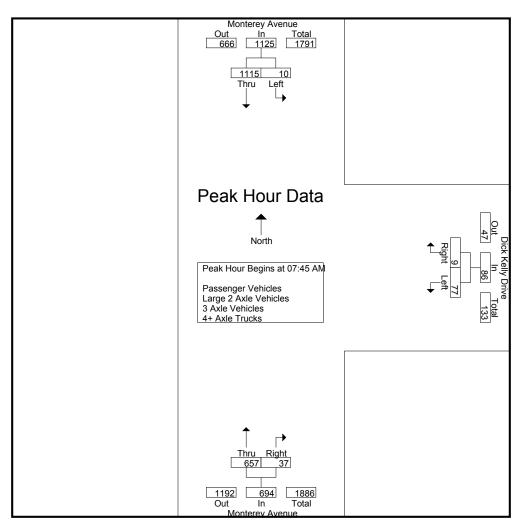
Groups Printed- Passenger Vehicles - Large 2 Axle Vehicles - 3 Axle Vehicles - 4+ Axle Trucks

| | | Ionterey Aver | nue | | Dick Kelly Driv | | Me | | | |
|-------------------------|------|---------------|------------|------|-----------------|------------|------|------------|------------|------------|
| | | Southbound | | | Westbound | | | Northbound | | |
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| 07:00 AM | 0 | 194 | 194 | 8 | 2 | 10 | 94 | 3 | 97 | 301 |
| 07:15 AM | 0 | 250 | 250 | 16 | 0 | 16 | 111 | 6 | 117 | 383 |
| 07:30 AM | 0 | 335 | 335 | 15 | 2 | 17 | 125 | 4 | 129 | 481 |
| 07:45 AM | 4 | 371 | 375 | 13 | 1_ | 14 | 142 | 7 | 149 | 538 |
| Total | 4 | 1150 | 1154 | 52 | 5 | 57 | 472 | 20 | 492 | 1703 |
| 00.00.444 | | 050 | 004 | 1 4- | | 40 | 404 | | 470 | 450 |
| 08:00 AM | 3 | 258 | 261 | 17 | 1 | 18 | 164 | 9 | 173 | 452 |
| 08:15 AM | 1 | 238 | 239 | 14 | 4 | 18 | 162 | 12 | 174 | 431 |
| 08:30 AM | 2 | 248 | 250 | 33 | 3 | 36 | 189 | 9 | 198 | 484 |
| 08:45 AM | 0 | 279 | 279 | 17 | 9 | 26 | 180 | 16 | 196 | 501_ |
| Total | 6 | 1023 | 1029 | 81 | 17 | 98 | 695 | 46 | 741 | 1868 |
| Grand Total | 10 | 2173 | 2183 | 133 | 22 | 155 | 1167 | 66 | 1233 | 3571 |
| Apprch % | 0.5 | 99.5 | 2100 | 85.8 | 14.2 | 100 | 94.6 | 5.4 | 1200 | 0071 |
| Total % | 0.3 | 60.9 | 61.1 | 3.7 | 0.6 | 4.3 | 32.7 | 1.8 | 34.5 | |
| Passenger Vehicles | 9 | 2091 | 2100 | 131 | 19 | 150 | 1116 | 64 | 1180 | 3430 |
| % Passenger Vehicles | 90 | 96.2 | 96.2 | 98.5 | 86.4 | 96.8 | 95.6 | 97 | 95.7 | 96.1 |
| Large 2 Axle Vehicles | 0 | 48 | 48 | 1 | 1 | 2 | 20 | 1 | 21 | 71 |
| % Large 2 Axle Vehicles | 0 | 2.2 | 2.2 | 0.8 | 4.5 | 1.3 | 1.7 | 1.5 | 1.7 | 2 |
| 3 Axle Vehicles | 0 | 24 | 24 | 0 | 0 | 0 | 17 | 0 | 17 | 41 |
| % 3 Axle Vehicles | 0 | 1.1 | 1.1 | 0 | 0 | 0 | 1.5 | 0 | 1.4 | 1.1_ |
| 4+ Axle Trucks | 1 | 10 | 11 | 1 | 2 | 3 | 14 | 1 | 15 | 29 |
| % 4+ Axle Trucks | 10 | 0.5 | 0.5 | 8.0 | 9.1 | 1.9 | 1.2 | 1.5 | 1.2 | 8.0 |

| | Monterey Avenue Southbound | | | | ck Kelly Driv Westbound | | Monterey Avenue Northbound Thru Right App. Total | | | Int. Total |
|----------------------------|-------------------------------|-----------------|-------------|------|----------------------------|-----|--------------------------------------------------|-----|-----|------------|
| Start Time | Left | Thru App. Total | | Left | Left Right App. Total | | | | | |
| Peak Hour Analysis From | n 07:00 AM to 0 | 08:45 AM - | Peak 1 of 1 | | - | | | - | | |
| Peak Hour for Entire Inter | rsection Begins | s at 07:45 A | AΜ | | | | | | | |
| 07:45 AM | 4 | 371 | 375 | 13 | 1 | 14 | 142 | 7 | 149 | 538 |
| 08:00 AM | 3 | 258 | 261 | 17 | 1 | 18 | 164 | 9 | 173 | 452 |
| 08:15 AM | 1 | 238 | 239 | 14 | 4 | 18 | 162 | 12 | 174 | 431 |
| 08:30 AM | 2 | 248 | 250 | 33 | 3 | 36 | 189 | 9 | 198 | 484 |
| Total Volume | 10 | 1115 | 1125 | 77 | 9 | 86 | 657 | 37 | 694 | 1905 |
| % App. Total | 0.9 | 99.1 | | 89.5 | 10.5 | | 94.7 | 5.3 | | |
| PHF | 625 | 751 | 750 | 583 | 563 | 597 | 869 | 771 | 876 | 885 |

City of Rancho Mirage N/S: Monterey Avenue E/W: Dick Kelly Drive Weather: Sunny

File Name: RNMMODKAM Site Code : 00000031 Start Date : 11/8/2012 Page No : 2



Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1

| Peak Hour | for | Each | App | oroach | Beg | ins at: |
|-----------|-----|------|-----|--------|-----|---------|
| | | | | | | |

| Peak Hour for Each App | roach Begins a | at: | | | | | | | | |
|------------------------|----------------|------|------|----------|------|------|----------|------|------|--|
| | 07:15 AM | | | 08:00 AM | | | 08:00 AM | | | |
| +0 mins. | 0 | 250 | 250 | 17 | 1 | 18 | 164 | 9 | 173 | |
| +15 mins. | 0 | 335 | 335 | 14 | 4 | 18 | 162 | 12 | 174 | |
| +30 mins. | 4 | 371 | 375 | 33 | 3 | 36 | 189 | 9 | 198 | |
| +45 mins. | 3 | 258 | 261 | 17 | 9 | 26 | 180 | 16 | 196 | |
| Total Volume | 7 | 1214 | 1221 | 81 | 17 | 98 | 695 | 46 | 741 | |
| % App. Total | 0.6 | 99.4 | | 82.7 | 17.3 | | 93.8 | 6.2 | | |
| PHF | .438 | .818 | .814 | .614 | .472 | .681 | .919 | .719 | .936 | |

City of Rancho Mirage N/S: Monterey Avenue E/W: Dick Kelly Drive Weather: Sunny

File Name: RNMMODKAM Site Code: 00000031

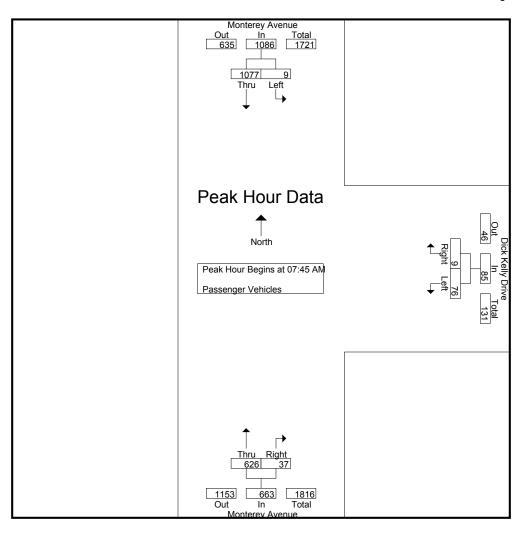
Start Date : 11/8/2012 Page No : 1

Groups Printed- Passenger Vehicles

| | | onterey Aven Southbound | | | ck Kelly Driv Westbound | /e | Monterey Avenue Northbound | | | |
|-------------------------|----------|----------------------------|------------|-------------|----------------------------|------------|-------------------------------|-----------|------------|------------|
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| 07:00 AM | 0 | 185 | 185 | 8 | 2 | 10 | 92 | 3 | 95 | 290 |
| 07:15 AM | Ö | 237 | 237 | 16 | 0 | 16 | 110 | 6 | 116 | 369 |
| 07:30 AM | 0 | 325 | 325 | 15 | 1 | 16 | 119 | 2 | 121 | 462 |
| 07:45 AM | 4 | 362 | 366 | 13 | 1 | 14 | 135 | 7 | 142 | 522 |
| Total | 4 | 1109 | 1113 | 52 | 4 | 56 | 456 | 18 | 474 | 1643 |
| 08:00 AM | 2 | 249 | 251 | 17 | 1 | 18 | 159 | 9 | 168 | 437 |
| 08:15 AM | 1 | 230 | 231 | 13 | 4 | 17 | 154 | 12 | 166 | 414 |
| 08:30 AM | 2 | 236 | 238 | 33 | 3 | 36 | 178 | 9 | 187 | 461 |
| 08:45 AM | 0 | 267 | 267 | 16 | 7 | 23 | 169 | 16 | 185 | 475 |
| Total | 5 | 982 | 987 | 79 | 15 | 94 | 660 | 46 | 706 | 1787 |
| Grand Total Apprch % | 9 0.4 | 2091 99.6 | 2100 | 131 87.3 | 19 12.7 | 150 | 1116 94.6 | 64 5.4 | 1180 | 3430 |
| Total % | 0.3 | 61 | 61.2 | 3.8 | 0.6 | 4.4 | 32.5 | 1.9 | 34.4 | |

| | - | nterey Aven Southbound | | | ck Kelly Driv Westbound | | M | ue | | |
|---------------------------|----------------|---------------------------|-------------|------|----------------------------|------------|------|-------|------------|------------|
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis Fron | n 07:45 AM to | 08:30 AM - I | Peak 1 of 1 | | - | | | - | | |
| Peak Hour for Entire Inte | rsection Begin | s at 07:45 A | .M | | | | | | | |
| 07:45 AM | 4 | 362 | 366 | 13 | 1 | 14 | 135 | 7 | 142 | 522 |
| 08:00 AM | 2 | 249 | 251 | 17 | 1 | 18 | 159 | 9 | 168 | 437 |
| 08:15 AM | 1 | 230 | 231 | 13 | 4 | 17 | 154 | 12 | 166 | 414 |
| 08:30 AM | 2 | 236 | 238 | 33 | 3 | 36 | 178 | 9 | 187 | 461_ |
| Total Volume | 9 | 1077 | 1086 | 76 | 9 | 85 | 626 | 37 | 663 | 1834 |
| % App. Total | 0.8 | 99.2 | | 89.4 | 10.6 | | 94.4 | 5.6 | | |
| PHF | .563 | .744 | .742 | .576 | .563 | .590 | .879 | .771 | .886 | .878 |

File Name: RNMMODKAM Site Code : 00000031 Start Date : 11/8/2012 Page No : 2



Peak Hour Analysis From 07:45 AM to 08:30 AM - Peak 1 of 1

| Peak Hour for Each App | roach Begins | at: | | | | | | | |
|------------------------|--------------|------|------|----------|------|------|----------|------|------|
| | 07:45 AM | | | 07:45 AM | | | 07:45 AM | | |
| +0 mins. | 4 | 362 | 366 | 13 | 1 | 14 | 135 | 7 | 142 |
| +15 mins. | 2 | 249 | 251 | 17 | 1 | 18 | 159 | 9 | 168 |
| +30 mins. | 1 | 230 | 231 | 13 | 4 | 17 | 154 | 12 | 166 |
| +45 mins. | 2 | 236 | 238 | 33 | 3 | 36 | 178 | 9 | 187 |
| Total Volume | 9 | 1077 | 1086 | 76 | 9 | 85 | 626 | 37 | 663 |
| % App. Total | 0.8 | 99.2 | | 89.4 | 10.6 | | 94.4 | 5.6 | |
| PHF | .563 | .744 | .742 | .576 | .563 | .590 | .879 | .771 | .886 |

City of Rancho Mirage N/S: Monterey Avenue E/W: Dick Kelly Drive Weather: Sunny

File Name: RNMMODKAM Site Code: 00000031

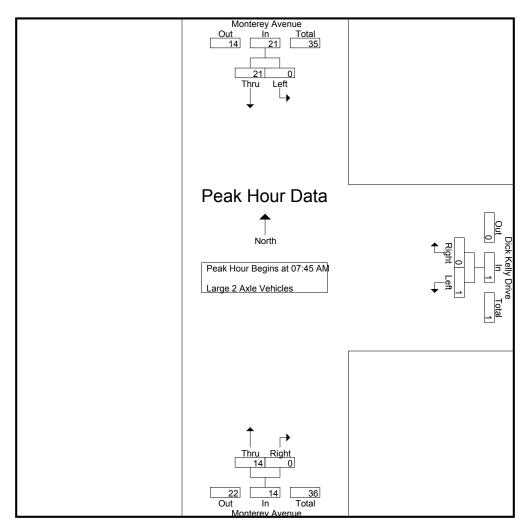
Start Date : 11/8/2012 Page No : 1

Groups Printed- Large 2 Axle Vehicles

| | | onterey Aven Southbound | | | ck Kelly Driv Westbound | /e | Mo | | | |
|-------------|------|----------------------------|------------|------|----------------------------|------------|------|-------|------------|------------|
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| 07:00 AM | 0 | 6 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 07:15 AM | 0 | 9 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 07:30 AM | 0 | 7 | 7 | 0 | 0 | 0 | 3 | 1 | 4 | 11 |
| 07:45 AM | 0 | 6 | 6 | 0 | 0 | 0 | 4 | 0 | 4 | 10 |
| Total | 0 | 28 | 28 | 0 | 0 | 0 | 7 | 1 | 8 | 36 |
| | | | | | | 1 | | | 1 | |
| 08:00 AM | 0 | 6 | 6 | 0 | 0 | 0 | 3 | 0 | 3 | 9 |
| 08:15 AM | 0 | 5 | 5 | 1 | 0 | 1 | 4 | 0 | 4 | 10 |
| 08:30 AM | 0 | 4 | 4 | 0 | 0 | 0 | 3 | 0 | 3 | 7 |
| 08:45 AM | 0 | 5 | 5 | 0 | 1 | 1 | 3 | 0 | 3 | 9_ |
| Total | 0 | 20 | 20 | 1 | 1 | 2 | 13 | 0 | 13 | 35 |
| | | | 1 | | | 1 | | | 1 | |
| Grand Total | 0 | 48 | 48 | 1 | 1 | 2 | 20 | 1 | 21 | 71 |
| Apprch % | 0 | 100 | | 50 | 50 | | 95.2 | 4.8 | | |
| Total % | 0 | 67.6 | 67.6 | 1.4 | 1.4 | 2.8 | 28.2 | 1.4 | 29.6 | |

| | | onterey Aven | | D | ick Kelly Dri | | Mo | iue | | |
|---------------------------|----------------|---------------|-------------|------|---------------|------------|------|-------|------------|------------|
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis Fron | n 07:45 AM to | 08:30 AM - F | Peak 1 of 1 | | - | | | - | | |
| Peak Hour for Entire Inte | rsection Begin | ns at 07:45 A | M | | | | | | | |
| 07:45 AM | 0 | 6 | 6 | 0 | 0 | 0 | 4 | 0 | 4 | 10 |
| 08:00 AM | 0 | 6 | 6 | 0 | 0 | 0 | 3 | 0 | 3 | 9 |
| 08:15 AM | 0 | 5 | 5 | 1 | 0 | 1 | 4 | 0 | 4 | 10 |
| 08:30 AM | 0 | 4 | 4 | 0 | 0 | 0 | 3 | 0 | 3 | 7_ |
| Total Volume | 0 | 21 | 21 | 1 | 0 | 1 | 14 | 0 | 14 | 36 |
| % App. Total | 0 | 100 | | 100 | 0 | | 100 | 0 | | |
| PHF | .000 | .875 | .875 | .250 | .000 | .250 | .875 | .000 | .875 | .900 |

File Name: RNMMODKAM Site Code : 00000031 Start Date : 11/8/2012 Page No : 2



Peak Hour Analysis From 07:45 AM to 08:30 AM - Peak 1 of 1

| Peak Hour for Each App | <u>roach Begins a</u> | at: | | | | | | | |
|------------------------|-----------------------|------|------|----------|------|------|----------|------|------|
| | 07:45 AM | | | 07:45 AM | | | 07:45 AM | | |
| +0 mins. | 0 | 6 | 6 | 0 | 0 | 0 | 4 | 0 | 4 |
| +15 mins. | 0 | 6 | 6 | 0 | 0 | 0 | 3 | 0 | 3 |
| +30 mins. | 0 | 5 | 5 | 1 | 0 | 1 | 4 | 0 | 4 |
| +45 mins. | 0 | 4 | 4 | 0 | 0 | 0 | 3 | 0 | 3 |
| Total Volume | 0 | 21 | 21 | 1 | 0 | 1 | 14 | 0 | 14 |
| % App. Total | 0 | 100 | | 100 | 0 | | 100 | 0 | |
| PHF | .000 | .875 | .875 | .250 | .000 | .250 | .875 | .000 | .875 |

City of Rancho Mirage N/S: Monterey Avenue E/W: Dick Kelly Drive Weather: Sunny

File Name: RNMMODKAM Site Code: 00000031

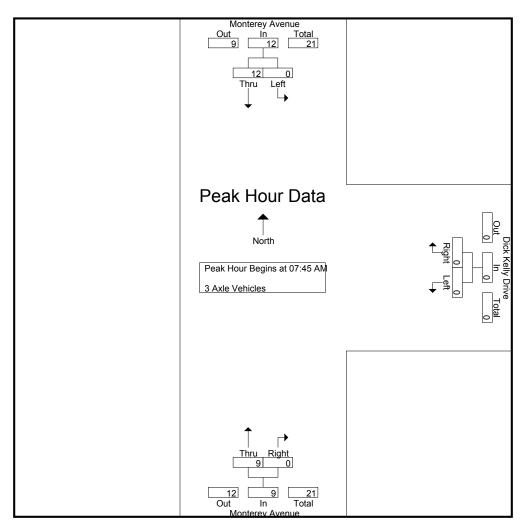
Start Date : 11/8/2012 Page No : 1

Groups Printed- 3 Axle Vehicles

| | | onterey Aven Southbound | | | ick Kelly Driv Westbound | /e | Мо | | | |
|-------------|------|----------------------------|------------|------|-----------------------------|------------|------|-------|------------|------------|
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| 07:00 AM | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 07:15 AM | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 07:30 AM | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 2 |
| 07:45 AM | 0 | 1_ | 1 | 0 | 0 | 0 | 2 | 0 | 2 | 3 |
| Total | 0 | 8 | 8 | 0 | 0 | 0 | 3 | 0 | 3 | 11 |
| | | | | | | | | | | |
| 08:00 AM | 0 | 2 | 2 | 0 | 0 | 0 | 2 | 0 | 2 | 4 |
| 08:15 AM | 0 | 2 | 2 | 0 | 0 | 0 | 1 | 0 | 1 | 3 |
| 08:30 AM | 0 | 7 | 7 | 0 | 0 | 0 | 4 | 0 | 4 | 11 |
| 08:45 AM | 0 | 5 | 5 | 0 | 0 | 0 | 7 | 0 | 7 | 12 |
| Total | 0 | 16 | 16 | 0 | 0 | 0 | 14 | 0 | 14 | 30 |
| | | | | | | | | | | |
| Grand Total | 0 | 24 | 24 | 0 | 0 | 0 | 17 | 0 | 17 | 41 |
| Apprch % | 0 | 100 | | 0 | 0 | | 100 | 0 | | |
| Total % | 0 | 58.5 | 58.5 | 0 | 0 | 0 | 41.5 | 0 | 41.5 | |

| | | onterey Aven | | Dick Kelly Drive Westbound | | | Mo | ue | | |
|---------------------------|----------------|---------------|-------------|-------------------------------|-------|------------|------|-------|------------|------------|
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis Fron | n 07:45 AM to | 08:30 AM - F | Peak 1 of 1 | | - | | | - | | |
| Peak Hour for Entire Inte | rsection Begin | ns at 07:45 A | M | | | | | | | |
| 07:45 AM | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 0 | 2 | 3 |
| 08:00 AM | 0 | 2 | 2 | 0 | 0 | 0 | 2 | 0 | 2 | 4 |
| 08:15 AM | 0 | 2 | 2 | 0 | 0 | 0 | 1 | 0 | 1 | 3 |
| 08:30 AM | 0 | 7 | 7 | 0 | 0 | 0 | 4 | 0 | 4 | 11_ |
| Total Volume | 0 | 12 | 12 | 0 | 0 | 0 | 9 | 0 | 9 | 21 |
| % App. Total | 0 | 100 | | 0 | 0 | | 100 | 0 | | |
| PHF | .000 | .429 | .429 | .000 | .000 | .000 | .563 | .000 | .563 | .477 |

File Name: RNMMODKAM Site Code : 00000031 Start Date : 11/8/2012 Page No : 2



Peak Hour Analysis From 07:45 AM to 08:30 AM - Peak 1 of 1

| Peak Hour for Each App | roach Begins | at: | | | | | | | |
|------------------------|--------------|------|------|----------|------|------|----------|------|------|
| | 07:45 AM | | | 07:45 AM | | | 07:45 AM | | |
| +0 mins. | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 0 | 2 |
| +15 mins. | 0 | 2 | 2 | 0 | 0 | 0 | 2 | 0 | 2 |
| +30 mins. | 0 | 2 | 2 | 0 | 0 | 0 | 1 | 0 | 1 |
| +45 mins. | 0 | 7 | 7 | 0 | 0 | 0 | 4 | 0 | 4 |
| Total Volume | 0 | 12 | 12 | 0 | 0 | 0 | 9 | 0 | 9 |
| % App. Total | 0 | 100 | | 0 | 0 | | 100 | 0 | |
| PHF | .000 | .429 | .429 | .000 | .000 | .000 | .563 | .000 | .563 |

City of Rancho Mirage N/S: Monterey Avenue E/W: Dick Kelly Drive Weather: Sunny

File Name: RNMMODKAM Site Code: 00000031

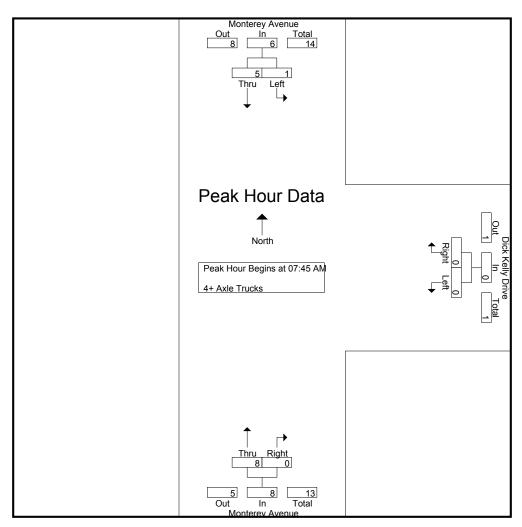
Start Date : 11/8/2012 Page No : 1

Groups Printed- 4+ Axle Trucks

| | | onterey Aven Southbound | | | Dick Kelly Driv Westbound | | | iue | | |
|-------------------------|----------|----------------------------|------------|-----------|------------------------------|------------|------------|----------|------------|------------|
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 2 |
| 07:15 AM | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 2 |
| 07:30 AM | 0 | 2 | 2 | 0 | 1 | 1 | 2 | 1 | 3 | 6 |
| 07:45 AM | 0 | 2 | 2 | 0 | 0 | 0 | 11 | 0 | 1 | 3 |
| Total | 0 | 5 | 5 | 0 | 1 | 1 | 6 | 1 | 7 | 13 |
| 08:00 AM | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 08:15 AM | 0 | 1 | 1 | 0 | 0 | 0 | 3 | 0 | 3 | 4 |
| 08:30 AM | 0 | 1 | 1 | 0 | 0 | 0 | 4 | 0 | 4 | 5 |
| 08:45 AM | 0 | 2 | 2 | 1 | 1 | 2 | 11 | 0 | 1 | 5_ |
| Total | 1 | 5 | 6 | 1 | 1 | 2 | 8 | 0 | 8 | 16 |
| Grand Total Apprch % | 1 9.1 | 10 90.9 | 11 | 1 33.3 | 2 66.7 | 3 | 14 93.3 | 1 6.7 | 15 | 29 |
| Total % | 3.4 | 34.5 | 37.9 | 3.4 | 6.9 | 10.3 | 48.3 | 3.4 | 51.7 | |

| | | onterey Avenu Southbound | ue | Dick Kelly Drive Westbound | | | Monterey Avenue Northbound | | | |
|---------------------------|----------------|-----------------------------|-------------|-------------------------------|-------|------------|-------------------------------|-------|------------|------------|
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis Fron | n 07:45 AM to | 08:30 AM - F | Peak 1 of 1 | | - | | | - | | |
| Peak Hour for Entire Inte | rsection Begin | ns at 07:45 Al | M . | | | | | | | |
| 07:45 AM | 0 | 2 | 2 | 0 | 0 | 0 | 1 | 0 | 1 | 3 |
| 08:00 AM | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 08:15 AM | 0 | 1 | 1 | 0 | 0 | 0 | 3 | 0 | 3 | 4 |
| 08:30 AM | 0 | 1 | 1 | 0 | 0 | 0 | 4 | 0 | 4 | 5_ |
| Total Volume | 1 | 5 | 6 | 0 | 0 | 0 | 8 | 0 | 8 | 14 |
| % App. Total | 16.7 | 83.3 | | 0 | 0 | | 100 | 0 | | |
| PHF | .250 | .625 | .750 | .000 | .000 | .000 | .500 | .000 | .500 | .700 |

File Name: RNMMODKAM Site Code : 00000031 Start Date : 11/8/2012 Page No : 2



Peak Hour Analysis From 07:45 AM to 08:30 AM - Peak 1 of 1

| Peal | ۲ŀ | lour | for | Each | nΑ | pp | roach | Beg | ins | at: |
|------|----|------|-----|------|----|----|-------|-----|-----|-----|
| | | | | | | | | | | |

| Peak Hour for Each App | roach Begins a | ıt: | | | | | | | |
|------------------------|----------------|------|------|----------|------|------|----------|------|------|
| | 07:45 AM | | | 07:45 AM | | | 07:45 AM | | |
| +0 mins. | 0 | 2 | 2 | 0 | 0 | 0 | 1 | 0 | 1 |
| +15 mins. | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| +30 mins. | 0 | 1 | 1 | 0 | 0 | 0 | 3 | 0 | 3 |
| +45 mins. | 0 | 1 | 1 | 0 | 0 | 0 | 4 | 0 | 4 |
| Total Volume | 1 | 5 | 6 | 0 | 0 | 0 | 8 | 0 | 8 |
| % App. Total | 16.7 | 83.3 | | 0 | 0 | | 100 | 0 | |
| PHF | .250 | .625 | .750 | .000 | .000 | .000 | .500 | .000 | .500 |

City of Rancho Mirage N/S: Monterey Avenue E/W: Dick Kelly Drive Weather: Sunny

File Name: RNMMODKPM Site Code: 00000031

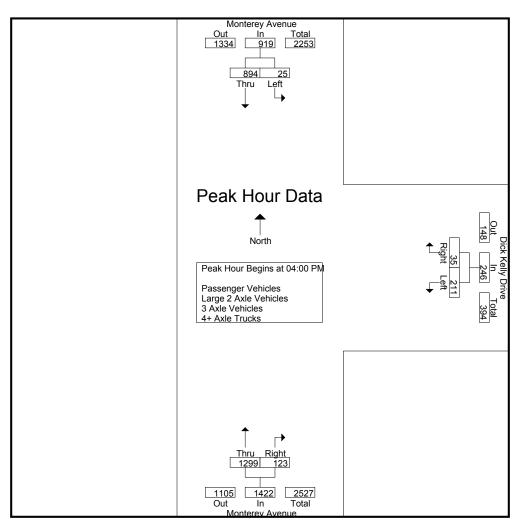
Start Date : 11/8/2012 Page No : 1

Groups Printed- Passenger Vehicles - Large 2 Axle Vehicles - 3 Axle Vehicles - 4+ Axle Trucks

| | Monterey Avenue | | | | Dick Kelly Dr | | Me | ue | | |
|-------------------------|-----------------|------------|------------|------|---------------|------------|------|------------|------------|------------|
| | | Southbound | | | Westbound | | | Northbound | | |
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| 04:00 PM | 7 | 230 | 237 | 57 | 10 | 67 | 348 | 31 | 379 | 683 |
| 04:15 PM | 10 | 211 | 221 | 48 | 9 | 57 | 311 | 25 | 336 | 614 |
| 04:30 PM | 5 | 225 | 230 | 50 | 7 | 57 | 321 | 39 | 360 | 647 |
| 04:45 PM | 3 | 228 | 231 | 56 | 9 | 65 | 319 | 28 | 347 | 643 |
| Total | 25 | 894 | 919 | 211 | 35 | 246 | 1299 | 123 | 1422 | 2587 |
| | | | | ı | | | 1 | | | |
| 05:00 PM | 2 | 217 | 219 | 53 | 7 | 60 | 308 | 27 | 335 | 614 |
| 05:15 PM | 4 | 202 | 206 | 40 | 17 | 57 | 367 | 23 | 390 | 653 |
| 05:30 PM | 4 | 193 | 197 | 38 | 14 | 52 | 256 | 22 | 278 | 527 |
| 05:45 PM | 2 | 195 | 197 | 39 | 5 | 44 | 244 | 18 | 262 | 503 |
| Total | 12 | 807 | 819 | 170 | 43 | 213 | 1175 | 90 | 1265 | 2297 |
| i | | | | ı | | | 1 | | | |
| Grand Total | 37 | 1701 | 1738 | 381 | 78 | 459 | 2474 | 213 | 2687 | 4884 |
| Apprch % | 2.1 | 97.9 | | 83 | 17 | | 92.1 | 7.9 | | |
| Total % | 0.8 | 34.8 | 35.6 | 7.8 | 1.6 | 9.4 | 50.7 | 4.4 | 55 | |
| Passenger Vehicles | 36 | 1677 | 1713 | 381 | 77 | 458 | 2428 | 212 | 2640 | 4811 |
| % Passenger Vehicles | 97.3 | 98.6 | 98.6 | 100 | 98.7 | 99.8 | 98.1 | 99.5 | 98.3 | 98.5 |
| Large 2 Axle Vehicles | 0 | 11 | 11 | 0 | 0 | 0 | 25 | 0 | 25 | 36 |
| % Large 2 Axle Vehicles | 0 | 0.6 | 0.6 | 0 | 0 | 0 | 1 | 0 | 0.9 | 0.7 |
| 3 Axle Vehicles | 0 | 10 | 10 | 0 | 0 | 0 | 17 | 1 | 18 | 28 |
| % 3 Axle Vehicles | 0 | 0.6 | 0.6 | 0 | 0 | 0 | 0.7 | 0.5 | 0.7 | 0.6 |
| 4+ Axle Trucks | 1 | 3 | 4 | 0 | 1 | 1 | 4 | 0 | 4 | 9 |
| % 4+ Axle Trucks | 2.7 | 0.2 | 0.2 | 0 | 1.3 | 0.2 | 0.2 | 0 | 0.1 | 0.2 |

| | Mor | nterey Aveni | ue | Di | ck Kelly Driv | ve | Mo | ue | | |
|-----------------------------|------------------|--------------|------------|------|---------------|------------|------|-------|------------|------------|
| | S | outhbound | | • | Westbound | | | | | |
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From (| 04:00 PM to 05:4 | 5 PM - Peal | k 1 of 1 | | | | | | | |
| Peak Hour for Entire Inters | ection Begins at | 04:00 PM | | | | | | | | |
| 04:00 PM | 7 | 230 | 237 | 57 | 10 | 67 | 348 | 31 | 379 | 683 |
| 04:15 PM | 10 | 211 | 221 | 48 | 9 | 57 | 311 | 25 | 336 | 614 |
| 04:30 PM | 5 | 225 | 230 | 50 | 7 | 57 | 321 | 39 | 360 | 647 |
| 04:45 PM | 3 | 228 | 231 | 56 | 9 | 65 | 319 | 28 | 347 | 643 |
| Total Volume | 25 | 894 | 919 | 211 | 35 | 246 | 1299 | 123 | 1422 | 2587 |
| % App. Total | 2.7 | 97.3 | | 85.8 | 14.2 | | 91.4 | 8.6 | | |
| PHF | .625 | .972 | .969 | .925 | .875 | .918 | .933 | .788 | .938 | .947 |

File Name: RNMMODKPM Site Code : 00000031 Start Date : 11/8/2012 Page No : 2



Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1

Peak Hour for Each Approach Begins at:
04:00 PM 04:30 PM 04:00 PM +0 mins. 230 237 57 10 67 321 39 360 +15 mins. 10 211 221 48 9 57 319 28 347 +30 mins. 57 225 230 308 27 335 50 5 +45 mins. 228 231 56 65 367 23 390 Total Volume 25 894 919 211 35 246 1315 117 1432 2.7 97.3 14.2 % App. Total 85.8 91.8 8.2 .969 .918 .918 PHF .625 .972 .925 .875 .896 .750

City of Rancho Mirage N/S: Monterey Avenue E/W: Dick Kelly Drive Weather: Sunny

File Name: RNMMODKPM Site Code: 00000031

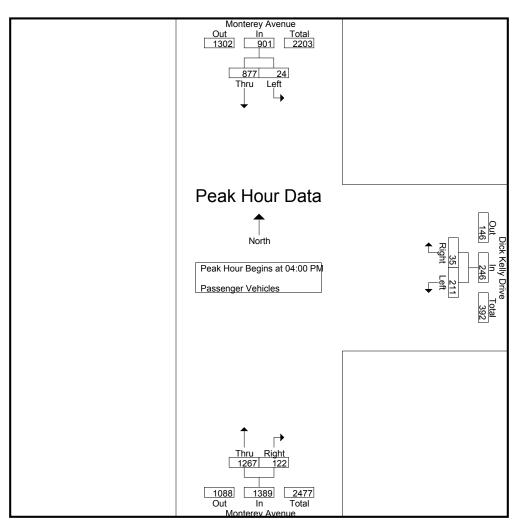
Start Date : 11/8/2012 Page No : 1

Groups Printed- Passenger Vehicles

| , | | | | oups i inica i i | | | | | | |
|-------------|-----------------|------------|------------|------------------|--------------|------------|------|--------------|------------|------------|
| | Monterey Avenue | | | Di | ck Kelly Dri | ve | Mo | onterey Aven | ue | |
| | | Southbound | | | Westbound | | | Northbound | | |
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| 04:00 PM | 7 | 217 | 224 | 57 | 10 | 67 | 339 | 31 | 370 | 661 |
| 04:15 PM | 10 | 210 | 220 | 48 | 9 | 57 | 304 | 24 | 328 | 605 |
| 04:30 PM | 5 | 224 | 229 | 50 | 7 | 57 | 312 | 39 | 351 | 637 |
| 04:45 PM | 2 | 226 | 228 | 56 | 9 | 65 | 312 | 28 | 340 | 633 |
| Total | 24 | 877 | 901 | 211 | 35 | 246 | 1267 | 122 | 1389 | 2536 |
| | | | | | | | | | | |
| 05:00 PM | 2 | 215 | 217 | 53 | 7 | 60 | 302 | 27 | 329 | 606 |
| 05:15 PM | 4 | 200 | 204 | 40 | 16 | 56 | 365 | 23 | 388 | 648 |
| 05:30 PM | 4 | 190 | 194 | 38 | 14 | 52 | 253 | 22 | 275 | 521 |
| 05:45 PM | 2 | 195 | 197 | 39 | 5 | 44 | 241 | 18 | 259 | 500 |
| Total | 12 | 800 | 812 | 170 | 42 | 212 | 1161 | 90 | 1251 | 2275 |
| | | | | | | | | | | |
| Grand Total | 36 | 1677 | 1713 | 381 | 77 | 458 | 2428 | 212 | 2640 | 4811 |
| Apprch % | 2.1 | 97.9 | | 83.2 | 16.8 | | 92 | 8 | | |
| Total % | 0.7 | 34.9 | 35.6 | 7.9 | 1.6 | 9.5 | 50.5 | 4.4 | 54.9 | |

| | Mor | nterey Avenu | ie | Di | ck Kelly Dri | ve | N | ue | | |
|-----------------------------|------------------|--------------|------------|------|--------------|------------|------|-------|------------|------------|
| | S | outhbound | | | Westbound | | | | | |
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From (| 04:00 PM to 04:4 | 5 PM - Peak | 1 of 1 | | | | | | | |
| Peak Hour for Entire Inters | ection Begins at | 04:00 PM | | | | | | | | |
| 04:00 PM | 7 | 217 | 224 | 57 | 10 | 67 | 339 | 31 | 370 | 661 |
| 04:15 PM | 10 | 210 | 220 | 48 | 9 | 57 | 304 | 24 | 328 | 605 |
| 04:30 PM | 5 | 224 | 229 | 50 | 7 | 57 | 312 | 39 | 351 | 637 |
| 04:45 PM | 2 | 226 | 228 | 56 | 9 | 65 | 312 | 28 | 340 | 633 |
| Total Volume | 24 | 877 | 901 | 211 | 35 | 246 | 1267 | 122 | 1389 | 2536 |
| % App. Total | 2.7 | 97.3 | | 85.8 | 14.2 | | 91.2 | 8.8 | | |
| PHF | .600 | .970 | .984 | .925 | .875 | .918 | .934 | .782 | .939 | .959 |

File Name: RNMMODKPM Site Code : 00000031 Start Date : 11/8/2012 Page No : 2



Peak Hour Analysis From 04:00 PM to 04:45 PM - Peak 1 of 1

| Peak Hour for Each Approx | ach Begins at: | | | | | | | | |
|---------------------------|----------------|------|------|----------|------|------|----------|------|------|
| | 04:00 PM | | | 04:00 PM | | | 04:00 PM | | |
| +0 mins. | 7 | 217 | 224 | 57 | 10 | 67 | 339 | 31 | 370 |
| +15 mins. | 10 | 210 | 220 | 48 | 9 | 57 | 304 | 24 | 328 |
| +30 mins. | 5 | 224 | 229 | 50 | 7 | 57 | 312 | 39 | 351 |
| +45 mins. | 2 | 226 | 228 | 56 | 9 | 65 | 312 | 28 | 340 |
| Total Volume | 24 | 877 | 901 | 211 | 35 | 246 | 1267 | 122 | 1389 |
| % App. Total | 2.7 | 97.3 | | 85.8 | 14.2 | | 91.2 | 8.8 | |
| PHF | .600 | .970 | .984 | .925 | .875 | .918 | .934 | .782 | .939 |

City of Rancho Mirage N/S: Monterey Avenue E/W: Dick Kelly Drive Weather: Sunny

File Name: RNMMODKPM Site Code: 00000031

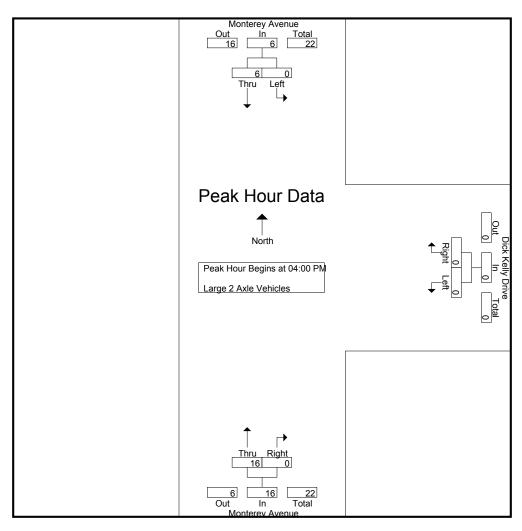
Start Date : 11/8/2012 Page No : 1

Groups Printed- Large 2 Axle Vehicles

| | | | Gro | ups Printed- La | rge 2 Axie Ve | enicles | | | | |
|-------------|------|--------------|------------|-----------------|---------------|------------|------|---------------|------------|------------|
| | Mor | nterey Avenu | ie | Di | ck Kelly Driv | re | Mo | onterey Avenu | e | |
| | S | Southbound | | | Westbound | | | Northbound | | |
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| 04:00 PM | 0 | 4 | 4 | 0 | 0 | 0 | 5 | 0 | 5 | 9 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 2 |
| 04:30 PM | 0 | 1 | 1 | 0 | 0 | 0 | 5 | 0 | 5 | 6 |
| 04:45 PM | 0 | 1 | 1 | 0 | 0 | 0 | 4 | 0 | 4 | 5_ |
| Total | 0 | 6 | 6 | 0 | 0 | 0 | 16 | 0 | 16 | 22 |
| | | | | | | | | | | |
| 05:00 PM | 0 | 2 | 2 | 0 | 0 | 0 | 3 | 0 | 3 | 5 |
| 05:15 PM | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 0 | 2 | 3 |
| 05:30 PM | 0 | 2 | 2 | 0 | 0 | 0 | 2 | 0 | 2 | 4 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 2 |
| Total | 0 | 5 | 5 | 0 | 0 | 0 | 9 | 0 | 9 | 14 |
| | | | | | | | | | | |
| Grand Total | 0 | 11 | 11 | 0 | 0 | 0 | 25 | 0 | 25 | 36 |
| Apprch % | 0 | 100 | | 0 | 0 | | 100 | 0 | | |
| Total % | 0 | 30.6 | 30.6 | 0 | 0 | 0 | 69.4 | 0 | 69.4 | |

| | Mo | nterey Avenu | ie | Ι | Dick Kelly Dri | ve | N | ue | | |
|-----------------------------|------------------|--------------|------------|-----------|----------------|------------|------|-------|------------|------------|
| | | Southbound | | Westbound | | | | | | |
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From (| 04:00 PM to 04: | 45 PM - Peak | 1 of 1 | | | | | | | |
| Peak Hour for Entire Inters | ection Begins at | 04:00 PM | | | | | | | | |
| 04:00 PM | 0 | 4 | 4 | 0 | 0 | 0 | 5 | 0 | 5 | 9 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 2 |
| 04:30 PM | 0 | 1 | 1 | 0 | 0 | 0 | 5 | 0 | 5 | 6 |
| 04:45 PM | 0 | 1 | 1 | 0 | 0 | 0 | 4 | 0 | 4 | 5_ |
| Total Volume | 0 | 6 | 6 | 0 | 0 | 0 | 16 | 0 | 16 | 22 |
| % App. Total | 0 | 100 | | 0 | 0 | | 100 | 0 | | |
| PHF | .000 | .375 | .375 | .000 | .000 | .000 | .800 | .000 | .800 | .611 |

File Name: RNMMODKPM Site Code : 00000031 Start Date : 11/8/2012 Page No : 2



Peak Hour Analysis From 04:00 PM to 04:45 PM - Peak 1 of 1

| Peak Hour for Each Approx | ach Begins at: | | | | | | | | |
|---------------------------|----------------|------|------|----------|------|------|----------|------|------|
| - | 04:00 PM | | | 04:00 PM | | | 04:00 PM | | |
| +0 mins. | 0 | 4 | 4 | 0 | 0 | 0 | 5 | 0 | 5 |
| +15 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 |
| +30 mins. | 0 | 1 | 1 | 0 | 0 | 0 | 5 | 0 | 5 |
| +45 mins. | 0 | 1 | 1 | 0 | 0 | 0 | 4 | 0 | 4 |
| Total Volume | 0 | 6 | 6 | 0 | 0 | 0 | 16 | 0 | 16 |
| % App. Total | 0 | 100 | | 0 | 0 | | 100 | 0 | |
| PHF | .000 | .375 | .375 | .000 | .000 | .000 | .800 | .000 | .800 |

City of Rancho Mirage N/S: Monterey Avenue E/W: Dick Kelly Drive Weather: Sunny

File Name: RNMMODKPM Site Code: 00000031

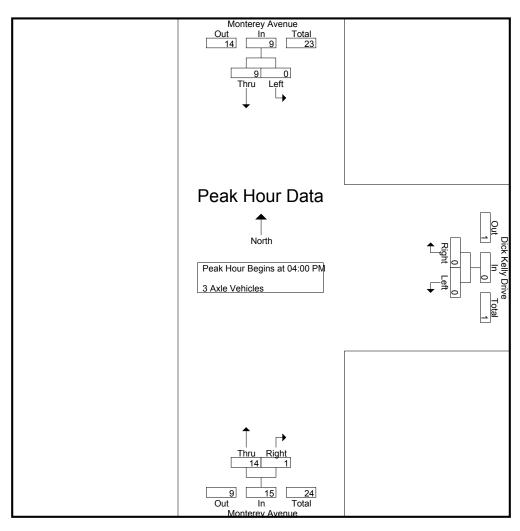
Start Date : 11/8/2012 Page No : 1

Groups Printed- 3 Axle Vehicles

| | | | | Groups Printed | - 3 Axie Veni | cies | | | | |
|-------------|------|--------------|------------|----------------|----------------|------------|------|---------------|------------|------------|
| | Mo | nterey Avenu | ie | D | ick Kelly Driv | ve | M | onterey Avenu | ie | |
| | | Southbound | | | Westbound | | | Northbound | | |
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| 04:00 PM | 0 | 8 | 8 | 0 | 0 | 0 | 3 | 0 | 3 | 11 |
| 04:15 PM | 0 | 1 | 1 | 0 | 0 | 0 | 4 | 1 | 5 | 6 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 4 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 3_ |
| Total | 0 | 9 | 9 | 0 | 0 | 0 | 14 | 1 | 15 | 24 |
| | | | | | | | | | | |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 3 |
| 05:15 PM | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0_ |
| Total | 0 | 1 | 1 | 0 | 0 | 0 | 3 | 0 | 3 | 4 |
| | | | | | | | | | | |
| Grand Total | 0 | 10 | 10 | 0 | 0 | 0 | 17 | 1 | 18 | 28 |
| Apprch % | 0 | 100 | | 0 | 0 | | 94.4 | 5.6 | | |
| Total % | 0 | 35.7 | 35.7 | 0 | 0 | 0 | 60.7 | 3.6 | 64.3 | |

| | M | onterey Aven | ue | I | Dick Kelly Dri | ve | M | ue | | |
|-----------------------------|-----------------|---------------|------------|------|----------------|------------|------|------------|------------|------------|
| | | Southbound | | | Westbound | | | Northbound | | |
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From (| 04:00 PM to 04 | :45 PM - Peal | k 1 of 1 | | | | | | | |
| Peak Hour for Entire Inters | ection Begins a | at 04:00 PM | | | | | | | | |
| 04:00 PM | 0 | 8 | 8 | 0 | 0 | 0 | 3 | 0 | 3 | 11 |
| 04:15 PM | 0 | 1 | 1 | 0 | 0 | 0 | 4 | 1 | 5 | 6 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 4 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 3_ |
| Total Volume | 0 | 9 | 9 | 0 | 0 | 0 | 14 | 1 | 15 | 24 |
| % App. Total | 0 | 100 | | 0 | 0 | | 93.3 | 6.7 | | |
| PHF | .000 | .281 | .281 | .000 | .000 | .000 | .875 | .250 | .750 | .545 |

File Name: RNMMODKPM Site Code : 00000031 Start Date : 11/8/2012 Page No : 2



Peak Hour Analysis From 04:00 PM to 04:45 PM - Peak 1 of 1

| Peak Hour for Each Approach Begins at: | | | | | | | | | | |
|----------------------------------------|----------|------|------|----------|------|------|----------|------|------|--|
| - | 04:00 PM | | | 04:00 PM | | | 04:00 PM | | | |
| +0 mins. | 0 | 8 | 8 | 0 | 0 | 0 | 3 | 0 | 3 | |
| +15 mins. | 0 | 1 | 1 | 0 | 0 | 0 | 4 | 1 | 5 | |
| +30 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | |
| +45 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | |
| Total Volume | 0 | 9 | 9 | 0 | 0 | 0 | 14 | 1 | 15 | |
| % App. Total | 0 | 100 | | 0 | 0 | | 93.3 | 6.7 | | |
| PHF | .000 | .281 | .281 | .000 | .000 | .000 | .875 | .250 | .750 | |

City of Rancho Mirage N/S: Monterey Avenue E/W: Dick Kelly Drive Weather: Sunny

File Name: RNMMODKPM Site Code: 00000031

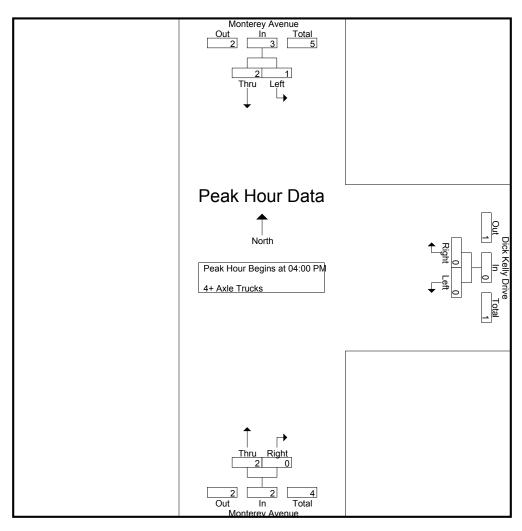
Start Date : 11/8/2012 Page No : 1

Groups Printed- 4+ Axle Trucks

| | | | | Groups Printea | - 4+ Axie 11u | icks | | | | |
|-------------|------|-------------|------------|----------------------|---------------|------------|-----------------|-------|------------|------------|
| | Mon | terey Avenu | ie | Dick Kelly Drive | | | Monterey Avenue | | | |
| | S | outhbound | | Westbound Northbound | | | | | | |
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| 04:00 PM | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 2 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Total | 1 | 2 | 3 | 0 | 0 | 0 | 2 | 0 | 2 | 5 |
| | | | | | | | | | | |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:15 PM | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 1 |
| 05:30 PM | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 2 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1_ |
| Total | 0 | 1 | 1 | 0 | 1 | 1 | 2 | 0 | 2 | 4 |
| | | | | | | | | | | |
| Grand Total | 1 | 3 | 4 | 0 | 1 | 1 | 4 | 0 | 4 | 9 |
| Apprch % | 25 | 75 | | 0 | 100 | | 100 | 0 | | |
| Total % | 11.1 | 33.3 | 44.4 | 0 | 11.1 | 11.1 | 44.4 | 0 | 44.4 | |

| | | onterey Aven Southbound | ue | Γ | Dick Kelly Dri Westbound | ve | Monterey Avenue Northbound | | | |
|-----------------------------|-----------------|----------------------------|------------|------|-----------------------------|------------|-------------------------------|-------|------------|------------|
| Start Time | Left | Thru | App. Total | Left | Right | App. Total | Thru | Right | App. Total | Int. Total |
| Peak Hour Analysis From (| 04:00 PM to 04: | 45 PM - Pea | k 1 of 1 | | | | | | | |
| Peak Hour for Entire Inters | ection Begins a | t 04:00 PM | | | | | | | | |
| 04:00 PM | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 2 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Total Volume | 1 | 2 | 3 | 0 | 0 | 0 | 2 | 0 | 2 | 5 |
| % App. Total | 33.3 | 66.7 | | 0 | 0 | | 100 | 0 | | |
| PHF | .250 | .500 | .375 | .000 | .000 | .000 | .500 | .000 | .500 | .625 |

File Name: RNMMODKPM Site Code : 00000031 Start Date : 11/8/2012 Page No : 2



Peak Hour Analysis From 04:00 PM to 04:45 PM - Peak 1 of 1

| Peak Hour for Each Approx | ach Begins at: | | | | | | | | |
|---------------------------|----------------|------|------|----------|------|------|----------|------|------|
| - | 04:00 PM | | | 04:00 PM | | | 04:00 PM | | |
| +0 mins. | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 | 1 |
| +15 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| +30 mins. | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| +45 mins. | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 1 | 2 | 3 | 0 | 0 | 0 | 2 | 0 | 2 |
| % App. Total | 33.3 | 66.7 | | 0 | 0 | | 100 | 0 | |
| PHF | .250 | .500 | .375 | .000 | .000 | .000 | .500 | .000 | .500 |

Coachella Valley Association of Governments (CVAG)
Daily Counts

Coachella Valley Association of Governments 2013 Traffic Census Report

| MONROE | S/O 54TH | 3,208 | 2013 | 17.20% |
|----------|-----------------|--------|------|---------|
| | | 2,387 | 2011 | -5.72% |
| | | 2,532 | 2010 | -13.19% |
| | | 2,917 | 2009 | -11.97% |
| | | 3,314 | 2008 | |
| | | | | |
| MONTEREY | S/O RAMON | 10,650 | 2013 | 7.59% |
| | | 9,246 | 2011 | -1.20% |
| | | 9,359 | 2010 | 13.74% |
| | | 8,228 | 2009 | -16.95% |
| | | 9,908 | 2008 | -4.35% |
| | | 10,359 | 2007 | 7.65% |
| | | 7,931 | 2003 | -23.96% |
| | | 10,431 | 2002 | 35.13% |
| | | 7,719 | 2001 | -13.30% |
| | | 8,904 | 2000 | 41.91% |
| | | 6,274 | 1999 | |
| | | | | |
| MONTEREY | N/O DINAH SHORE | 44,125 | 2013 | 2.88% |
| | | 41,725 | 2011 | 2.26% |
| | | 40,800 | 2010 | -1.46% |
| | | 41,405 | 2009 | -2.85% |
| | | 42,620 | 2008 | -0.97% |
| | | 43,039 | 2007 | 21.89% |
| | | 35,309 | 2006 | 4.72% |
| | | 29,700 | 2002 | -8.83% |
| | | 32,578 | 2001 | 6.29% |
| | | 30,649 | 2000 | 14.69% |
| | | 26,722 | 1999 | |
| | | | | |
| MONTEREY | S/O DINAH SHORE | 31,702 | 2013 | 0.99% |
| | | 31,085 | 2011 | 6.95% |
| | | 29,064 | 2010 | 2.71% |
| | | 28,296 | 2009 | -17.20% |
| | | 34,177 | 2008 | -3.05% |
| | | 35,253 | 2007 | 10.00% |
| | | 32,048 | 2006 | -3.68% |
| | | 33,275 | 2005 | 6.52% |
| | | 31,236 | 2004 | 3.87% |
| | | 28,992 | 2002 | |
| | | | | |

Coachella Valley Association of Governments 2013 Traffic Census Report

| MONTEREY | N/O GERALD FORD | 30,797 | 2013 | 4.62% |
|----------|-------------------|--------|------|---------|
| | | 28,190 | 2011 | 3.73% |
| | | 27,176 | 2010 | -5.04% |
| | | 28,620 | 2009 | -18.45% |
| | | 35,099 | 2008 | 7.42% |
| | | 32,673 | 2007 | 0.49% |
| | | 32,511 | 2006 | -14.76% |
| | | 38,142 | 2005 | 17.83% |
| | | 32,368 | 2004 | 3.45% |
| | | 31,288 | 2003 | 4.96% |
| | | 29,809 | 2002 | |
| | | | | |
| MONTEREY | S/O GERALD FORD | 25,531 | 2013 | -3.50% |
| | | 27,454 | 2011 | 6.31% |
| | | 25,824 | 2010 | -16.98% |
| | | 31,106 | 2009 | -6.18% |
| | | 33,158 | 2008 | -1.81% |
| | | 33,771 | 2007 | 5.16% |
| | | 32,111 | 2006 | -17.77% |
| | | 39,051 | 2005 | 5.82% |
| | | 36,902 | 2004 | |
| | | | | |
| MONTEREY | N/O FRANK SINATRA | 34,201 | 2013 | 9.76% |
| | | 28,617 | 2011 | 9.22% |
| | | 26,200 | 2010 | -6.39% |
| | | 27,991 | 2009 | -10.84% |
| | | 31,397 | 2008 | -4.01% |
| | | 32,709 | 2007 | -1.92% |
| | | 33,352 | 2006 | -12.97% |
| | | 38,326 | 2005 | 0.14% |
| | | 38,270 | 2004 | 3.53% |
| | | 36,962 | 2003 | 10.38% |
| | | 24,329 | 1998 | |

Peak Hour to Daily Traffic Volume Relationship

EXISTING PEAK HOUR-TO-DAILY TRAFFIC VOLUME RELATIONSHIP

| ţi | | |
|------------------------------|---------------------|---------------------|
| PM Ratio | 0.07 | 0.08 |
| PM Peak Hour Count (2012) | 2,297 | 2,570 |
| AM Ratio | 90'0 | 90'0 |
| AM Peak Hour Count (2012) | 1,858 | 1,952 |
| CVAG 2013 ADT | 31,702 | 262'08 |
| LEG | s/o Dinah Shore Dr. | n/o Gerald Ford Dr. |
| Roadway/Segment | Montorov | Molicies Av. |

ADT CALCULATION FACTOR

7.1940

7.80%

6.10%

3,810AVERAGE

62,499

TOTAL

4,867

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ATTACHMENT B

Existing (2012) Conditions Intersection Operations Analysis Worksheets

| | • | • | ₹I | † | / | > | ļ | |
|--------------------------------|------------|------|-------|----------|------------|-------------|----------|--|
| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT | |
| Lane Configurations | ሻ | 7 | Ð | ተተተ | 7 | ሻ | ^ | |
| Volume (vph) | 78 | 9 | 0 | 689 | 37 | 12 | 1148 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Total Lost time (s) | 4.0 | 4.0 | | 5.0 | 5.0 | 4.0 | 5.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 0.91 | 1.00 | 1.00 | 0.95 | |
| Frt | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 1.00 | |
| Flt Protected | 0.95 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1805 | 1615 | | 5187 | 1615 | 1805 | 3610 | |
| Flt Permitted | 0.95 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1805 | 1615 | | 5187 | 1615 | 1805 | 3610 | |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | |
| Adj. Flow (vph) | 88 | 10 | 0 | 774 | 42 | 13 | 1290 | |
| RTOR Reduction (vph) | 0 | 9 | 0 | 0 | 9 | 0 | 0 | |
| Lane Group Flow (vph) | 88 | 1 | 0 | 774 | 33 | 13 | 1290 | |
| Turn Type | NA | Perm | Prot | NA | Perm | Prot | NA | |
| Protected Phases | 3 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | | 3 | | | 6 | | | |
| Actuated Green, G (s) | 9.3 | 9.3 | | 95.5 | 95.5 | 2.2 | 101.7 | |
| Effective Green, g (s) | 9.3 | 9.3 | | 95.5 | 95.5 | 2.2 | 101.7 | |
| Actuated g/C Ratio | 0.08 | 0.08 | | 0.80 | 0.80 | 0.02 | 0.85 | |
| Clearance Time (s) | 4.0 | 4.0 | | 5.0 | 5.0 | 4.0 | 5.0 | |
| Vehicle Extension (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | 1.0 | |
| Lane Grp Cap (vph) | 139 | 125 | | 4127 | 1285 | 33 | 3059 | |
| v/s Ratio Prot | c0.05 | | | 0.15 | | 0.01 | c0.36 | |
| v/s Ratio Perm | | 0.00 | | | 0.02 | | | |
| v/c Ratio | 0.63 | 0.01 | | 0.19 | 0.03 | 0.39 | 0.42 | |
| Uniform Delay, d1 | 53.7 | 51.1 | | 2.9 | 2.6 | 58.2 | 2.2 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 6.7 | 0.0 | | 0.1 | 0.0 | 2.8 | 0.4 | |
| Delay (s) | 60.4 | 51.1 | | 3.0 | 2.6 | 61.0 | 2.6 | |
| Level of Service | Е | D | | Α | Α | Е | Α | |
| Approach Delay (s) | 59.5 | | | 3.0 | | | 3.2 | |
| Approach LOS | Е | | | Α | | | Α | |
| Intersection Summary | | | | | | | | |
| HCM 2000 Control Delay | | | 5.6 | H | CM 2000 | Level of | Service | |
| HCM 2000 Volume to Capac | city ratio | | 0.46 | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | Sı | um of lost | time (s) | | |
| Intersection Capacity Utilizat | tion | | 43.6% | IC | CU Level c | of Service | : | |
| Analysis Period (min) | | | 15 | | | | | |
| c Critical Lane Group | | | | | | | | |

| | • | • | ₹I | † | / | > | ↓ |
|-------------------------------|------------|------|-------|----------|------------|-------------|----------|
| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |
| Lane Configurations | ሻ | 7 | Ð | ተተተ | 7 | ሻ | ^ |
| Volume (vph) | 211 | 35 | 0 | 1325 | 124 | 27 | 910 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 5.0 | 5.0 | 4.0 | 5.0 |
| Lane Util. Factor | 1.00 | 1.00 | | 0.91 | 1.00 | 1.00 | 0.95 |
| Frt | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 1.00 |
| Flt Protected | 0.95 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 1805 | 1615 | | 5187 | 1615 | 1805 | 3610 |
| Flt Permitted | 0.95 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (perm) | 1805 | 1615 | | 5187 | 1615 | 1805 | 3610 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 222 | 37 | 0 | 1395 | 131 | 28 | 958 |
| RTOR Reduction (vph) | 0 | 32 | 0 | 0 | 37 | 0 | 0 |
| Lane Group Flow (vph) | 222 | 5 | 0 | 1395 | 94 | 28 | 958 |
| Turn Type | NA | Perm | Prot | NA | Perm | Prot | NA |
| Protected Phases | 3 | | 1 | 6 | | 5 | 2 |
| Permitted Phases | | 3 | | | 6 | | |
| Actuated Green, G (s) | 17.1 | 17.1 | | 86.0 | 86.0 | 3.9 | 93.9 |
| Effective Green, g (s) | 17.1 | 17.1 | | 86.0 | 86.0 | 3.9 | 93.9 |
| Actuated g/C Ratio | 0.14 | 0.14 | | 0.72 | 0.72 | 0.03 | 0.78 |
| Clearance Time (s) | 4.0 | 4.0 | | 5.0 | 5.0 | 4.0 | 5.0 |
| Vehicle Extension (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | 1.0 |
| Lane Grp Cap (vph) | 257 | 230 | | 3717 | 1157 | 58 | 2824 |
| v/s Ratio Prot | c0.12 | | | c0.27 | | c0.02 | 0.27 |
| v/s Ratio Perm | | 0.00 | | | 0.06 | | |
| v/c Ratio | 0.86 | 0.02 | | 0.38 | 0.08 | 0.48 | 0.34 |
| Uniform Delay, d1 | 50.3 | 44.3 | | 6.6 | 5.1 | 57.1 | 3.9 |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 23.9 | 0.0 | | 0.3 | 0.1 | 2.3 | 0.3 |
| Delay (s) | 74.2 | 44.3 | | 6.9 | 5.3 | 59.4 | 4.2 |
| Level of Service | Е | D | | А | Α | E | Α |
| Approach Delay (s) | 69.9 | | | 6.7 | | | 5.8 |
| Approach LOS | Е | | | Α | | | Α |
| Intersection Summary | | | | | | | |
| HCM 2000 Control Delay | | | 12.3 | Н | CM 2000 | Level of S | Service |
| HCM 2000 Volume to Capac | city ratio | | 0.46 | | | | |
| Actuated Cycle Length (s) | | | 120.0 | S | um of lost | t time (s) | |
| Intersection Capacity Utiliza | tion | | 44.8% | IC | CU Level | of Service | |
| Analysis Period (min) | | | 15 | | | | |
| c Critical Lane Group | | | | | | | |

ATTACHMENT C

Existing (2012) Conditions Queuing Analysis Worksheets

Queues

1: Monterey Av. (NS) & Dick Kelly Dr. (EW)

| | • | • | ₹N | † | / | - | ļ |
|-------------------------|------|------|------|----------|------|------|----------|
| Lane Group | WBL | WBR | NBU | NBT | NBR | SBL | SBT |
| Lane Configurations | ሻ | 7 | Ð | ተተተ | 7 | ٦ | ^ |
| Volume (vph) | 78 | 9 | 0 | 689 | 37 | 12 | 1148 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 | 0 | 205 | | 220 | 250 | |
| Storage Lanes | 1 | 1 | 1 | | 1 | 1 | |
| Taper Length (ft) | 90 | | 90 | | | 90 | |
| Right Turn on Red | | Yes | | | Yes | | |
| Link Speed (mph) | 45 | | | 55 | | | 55 |
| Link Distance (ft) | 1355 | | | 2143 | | | 1222 |
| Travel Time (s) | 20.5 | | | 26.6 | | | 15.1 |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Adj. Flow (vph) | 88 | 10 | 0 | 774 | 42 | 13 | 1290 |
| Shared Lane Traffic (%) | | | | | | | |
| Lane Group Flow (vph) | 88 | 10 | 0 | 774 | 42 | 13 | 1290 |
| v/c Ratio | 0.63 | 0.07 | | 0.18 | 0.03 | 0.17 | 0.42 |
| Control Delay | 72.8 | 25.2 | | 3.1 | 1.4 | 60.0 | 2.8 |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 72.8 | 25.2 | | 3.1 | 1.4 | 60.0 | 2.8 |
| Queue Length 50th (ft) | 67 | 0 | | 28 | 0 | 10 | 90 |
| Queue Length 95th (ft) | 117 | 17 | | 74 | 9 | 31 | 145 |
| Internal Link Dist (ft) | 1275 | | | 2063 | | | 1142 |
| Turn Bay Length (ft) | | | | | 220 | 250 | |
| Base Capacity (vph) | 240 | 224 | | 4231 | 1325 | 120 | 3059 |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.37 | 0.04 | | 0.18 | 0.03 | 0.11 | 0.42 |
| Intersection Summary | | | | | | | |

Area Type:

Other

| | • | • | ₹I | † | / | > | ļ |
|-------------------------|------|------|------|----------|----------|-------------|----------|
| Lane Group | WBL | WBR | NBU | NBT | NBR | SBL | SBT |
| Lane Configurations | * | 7 | Ð | ተተተ | 7 | * | ^ |
| Volume (vph) | 211 | 35 | 0 | 1325 | 124 | 27 | 910 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 | 0 | 205 | | 220 | 250 | |
| Storage Lanes | 1 | 1 | 1 | | 1 | 1 | |
| Taper Length (ft) | 90 | | 90 | | | 90 | |
| Right Turn on Red | | Yes | | | Yes | | |
| Link Speed (mph) | 45 | | | 55 | | | 55 |
| Link Distance (ft) | 1355 | | | 2143 | | | 1222 |
| Travel Time (s) | 20.5 | | | 26.6 | | | 15.1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Adj. Flow (vph) | 222 | 37 | 0 | 1395 | 131 | 28 | 958 |
| Shared Lane Traffic (%) | | | | | | | |
| Lane Group Flow (vph) | 222 | 37 | 0 | 1395 | 131 | 28 | 958 |
| v/c Ratio | 0.86 | 0.14 | | 0.37 | 0.11 | 0.32 | 0.34 |
| Control Delay | 80.8 | 15.4 | | 6.8 | 1.2 | 64.3 | 4.3 |
| Queue Delay | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 80.8 | 15.4 | | 6.8 | 1.2 | 64.3 | 4.3 |
| Queue Length 50th (ft) | 168 | 0 | | 150 | 0 | 22 | 103 |
| Queue Length 95th (ft) | #318 | 32 | | 175 | 18 | 52 | 113 |
| Internal Link Dist (ft) | 1275 | | | 2063 | | | 1142 |
| Turn Bay Length (ft) | | | | | 220 | 250 | |
| Base Capacity (vph) | 262 | 265 | | 3788 | 1215 | 120 | 2825 |
| Starvation Cap Reductn | 0 | 0 | | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.85 | 0.14 | | 0.37 | 0.11 | 0.23 | 0.34 |
| Intersection Summary | | | | | | | |

Intersection Summary

Area Type: Other

Queue shown is maximum after two cycles.

^{# 95}th percentile volume exceeds capacity, queue may be longer.

ATTACHMENT D

Long Range (2035) Growth Reasonableness Review Summary

EXISTING (2012) VS LONG RANGE (2035) GROWTH COMPARISON

11/8/2012

AM/PM Count Date:

1: Monterey Avenue / Dick Kelly Drive

TOTAL 2,655 2,778 2,632 5,287 101% WBR 0.947 557% 230 195 35 52 PHF: 100% 105 105 0 0 WBL 35% 211 285 217 74 EBR 100% 182 182 0 100% EBT 135 135 0 0 100% EBL 220 220 0 0 PM PEAK HOUR SBR 100% 132 132 0 SBT 1,476 62% 999 910 626 SBL 822% 249 222 46 27 126% NBT NBR 280 156 138 124 1,366 1,325 1,791 35% 466 NBU∗ 100% 202 202 0 TOTAL 1,973 3,657 1,684 2,095 85% ΑM 0.885 WBR 1044% 103 94 17 100% 품: WBT 100 100 0 WBL 29% 101 23 78 8 100% EBR 34 34 0 0 100% EBT 0 7 100% EBL 0 41 41 0 AM PEAK HOUR SBR 100% 36 36 0 1,189 1,622 SBT 41% 474 SBL 675% 19 12 93 8 NBR %659 244 281 37 28 1,189 NBT 73% 200 689 732 NBU⁴ 100% 55 22 0 0 2014 (Interpolate) 2035 Volumes Existing 2012 Growth % Delta

* NBU = NB U-Turn Only

| | | al | 7 | 34 | 7 | % | | | |
|---------------------------|--------------|-----------------------------------------------------|------------------------------------------------|---------------------------------------------------------------|-----------------------------------------------------|--------------------------------------------------------------------------------------------|--|-----|-----|
| | fed. | r Tot | 397 | 1,28 | 88 | % 223 | | | |
| | East Leg | LOO | 151 | 664 | 513 | 3409 | | | |
| | | <u></u> | 0 246 151 | 620 | 374 | 152% | | | |
| nmes | 5g | Total | 0 | 976 | 9/6 | 100% | | | |
| nk Vol | West Leg | TUO | 0 | 439 | 436 | 100% | | | |
| eak Hour | <u>N</u> | 0 | 537 | 537 | 100% | | | | |
| Peak I | g | IN OUT Total IN OUT Total IN OUT Total IN OUT Total | 2,297 | 4,098 | 1,801 | 73% 64% 98% 65% 78% 100% 100% 100% 152% 340% 223% | | | |
| PM | North Leg | OUT | 1,360 | 2,241 | 881 | 65% | | | |
| | ž | <u>N</u> | 937 | 1,857 | 920 | %86 | | | |
| |) | Total | 2,570 | 4,216 | 1,646 | 64% | | | |
| | South Leg | OUT | 1,121 | 1,943 | 822 | 73% | | | |
| | So | Z | 1,449 1,121 2,570 937 1,360 2,297 0 | 2,273 1,943 4,216 1,857 2,241 4,098 537 439 976 620 664 1,284 | 824 822 1,646 920 881 1,801 537 439 976 374 513 887 | 21% | | | |
| | | | | | | | | | |
| East Leg | g | Total | 136 | 089 | 544 | 400% | | | |
| | OUT | 46 | 376 | 327 | %199 | | | | |
| | N | 87 | 304 | 217 | 249% | | | | |
| |) | Total | 0 | 268 | 268 | 100% | | | |
| | West Leg | OUT | 0 | | 191 | 100% | | | |
| olumes | W | N | 0 | 191 | 77 | 100% | | | |
| AM Peak Hour Link Volumes | otal ,858 | | 799 531 1,330 591 635 1,226 77 191 268 217 327 | 66% 100% 100% 100% 249% 667% 400% | | | | | |
| eak Hou | North Leg | North Le | | 1,333 | 635 | 91% | | | |
| AM P | | Nor | No | No | Nor | NO IN O 1,160 6 1,751 1, | | 591 | 21% |
| | | Fotal | ,952 | 3,282 | 1,330 | %89 | | | |
| | South Leg | TUC | ,226 | 3757 | 531 | 13% | | | |
| | Sou | N | 726 1 | 1,525 | 662 | 110% 43% 68% 51% 91% | | | |
| | | | Existing 2012 | 2035 Volumes | Delta | Growth % | | | |

| | | ADT | | |
|----------------------------|-----------|-----------|----------|----------|
| | South Leg | North Leg | West Leg | East Leg |
| Existing 2012 ¹ | 32,531 | 29,891 | 0 | 3,834 |
| 2035 ADT | 29,600 | 61,800 | 6,700 | 13,400 |
| Delta | 27,069 | 31,909 | 6,700 | 995'6 |
| Growth % | 83% | 107% | 100% | 250% |
| 2014 (Interpolate) | 34,885 | 32,666 | 0 | 4,666 |

| | TRUCK (| TRUCK (4%) ADT | |
|-----------|-----------|----------------|----------|
| South Leg | North Leg | West Leg | East Leg |
| 1,301 | 1,196 | 0 | 153 |
| 2,384 | 2,472 | 268 | 536 |
| 1,083 | 1,276 | 368 | 383 |
| 83% | 107% | 100% | 720% |
| 1,395 | 1,307 | 0 | 187 |

Existing ADT Factor = 7.1940

ADT Factor based on CVAG ADT (2013) and Peak hour Counts collected for Urban Crossroads (11/2012). See Existing-to-daily peak hour relationship calc.

¹ Existing ADT Calc: ((AM+PM Peak Link Volume) * ADT Factor)

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ATTACHMENT E

Long Range (2035) Without Widening Conditions Intersection Operations Analysis Worksheets

| | ۶ | → | \rightarrow | • | ← | • | • | † | / | > | ļ | 4 |
|--------------------------------|------------|----------|---------------|-------|------------|------------|---------|----------|------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | † | 7 | J. | f) | | J. | ተተተ | 7 | J. | ^ | 7 |
| Volume (vph) | 41 | 2 | 34 | 101 | 100 | 103 | 55 | 1189 | 281 | 93 | 1622 | 36 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1805 | 1900 | 1615 | 1805 | 1755 | | 1805 | 5187 | 1615 | 1805 | 3610 | 1615 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1805 | 1900 | 1615 | 1805 | 1755 | | 1805 | 5187 | 1615 | 1805 | 3610 | 1615 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 41 | 2 | 34 | 101 | 100 | 103 | 55 | 1189 | 281 | 93 | 1622 | 36 |
| RTOR Reduction (vph) | 0 | 0 | 31 | 0 | 37 | 0 | 0 | 0 | 122 | 0 | 0 | 14 |
| Lane Group Flow (vph) | 41 | 2 | 3 | 101 | 166 | 0 | 55 | 1189 | 159 | 93 | 1622 | 22 |
| Turn Type | Prot | NA | Perm | Prot | NA | | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 7 | 4 | | 3 | 8 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | | | 4 | | | | | | 6 | | | 2 |
| Actuated Green, G (s) | 7.1 | 10.2 | 10.2 | 14.2 | 17.3 | | 7.6 | 67.8 | 67.8 | 11.8 | 72.0 | 72.0 |
| Effective Green, g (s) | 7.1 | 10.2 | 10.2 | 14.2 | 17.3 | | 7.6 | 67.8 | 67.8 | 11.8 | 72.0 | 72.0 |
| Actuated g/C Ratio | 0.06 | 0.08 | 0.08 | 0.12 | 0.14 | | 0.06 | 0.56 | 0.56 | 0.10 | 0.60 | 0.60 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 1.0 | 1.0 | 1.0 | 3.0 | | 3.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lane Grp Cap (vph) | 106 | 161 | 137 | 213 | 253 | | 114 | 2930 | 912 | 177 | 2166 | 969 |
| v/s Ratio Prot | 0.02 | 0.00 | | c0.06 | c0.09 | | 0.03 | 0.23 | | c0.05 | c0.45 | |
| v/s Ratio Perm | | | 0.00 | | | | | | 0.10 | | | 0.01 |
| v/c Ratio | 0.39 | 0.01 | 0.02 | 0.47 | 0.66 | | 0.48 | 0.41 | 0.17 | 0.53 | 0.75 | 0.02 |
| Uniform Delay, d1 | 54.4 | 50.3 | 50.3 | 49.4 | 48.5 | | 54.3 | 14.7 | 12.6 | 51.4 | 17.4 | 9.7 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 2.3 | 0.0 | 0.0 | 0.6 | 6.0 | | 3.2 | 0.4 | 0.4 | 1.3 | 2.4 | 0.0 |
| Delay (s) | 56.7 | 50.3 | 50.3 | 50.0 | 54.6 | | 57.5 | 15.1 | 13.0 | 52.7 | 19.9 | 9.8 |
| Level of Service | E | D | D | D | D | | Е | В | В | D | В | Α |
| Approach Delay (s) | | 53.7 | | | 53.1 | | | 16.3 | | | 21.4 | |
| Approach LOS | | D | | | D | | | В | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 22.6 | Н | CM 2000 | Level of S | Service | | С | | | |
| HCM 2000 Volume to Capac | city ratio | | 0.72 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | | um of lost | | | | 16.0 | | | |
| Intersection Capacity Utilizat | ion | | 76.4% | IC | CU Level o | of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| | ٠ | - | • | • | ← | • | • | † | / | > | ţ | 4 |
|-------------------------------|-------------|----------|-------|-------|-------------|------------|---------|----------|------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ň | † | 7 | 7 | f) | | 7 | ተተተ | 7 | Ţ | ^ | 7 |
| Volume (vph) | 220 | 135 | 182 | 285 | 105 | 230 | 202 | 1791 | 280 | 249 | 1476 | 132 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.90 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1805 | 1900 | 1615 | 1805 | 1704 | | 1805 | 5187 | 1615 | 1805 | 3610 | 1615 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1805 | 1900 | 1615 | 1805 | 1704 | | 1805 | 5187 | 1615 | 1805 | 3610 | 1615 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 220 | 135 | 182 | 285 | 105 | 230 | 202 | 1791 | 280 | 249 | 1476 | 132 |
| RTOR Reduction (vph) | 0 | 0 | 136 | 0 | 74 | 0 | 0 | 0 | 107 | 0 | 0 | 45 |
| Lane Group Flow (vph) | 220 | 135 | 46 | 285 | 261 | 0 | 202 | 1791 | 173 | 249 | 1476 | 87 |
| Turn Type | Prot | NA | Perm | Prot | NA | | Prot | NA | Perm | Prot | NA | Perm |
| Protected Phases | 7 | 4 | | 3 | 8 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | | | 4 | | | | | | 6 | | | 2 |
| Actuated Green, G (s) | 15.0 | 21.3 | 21.3 | 17.0 | 23.3 | | 12.0 | 56.7 | 56.7 | 9.0 | 53.7 | 53.7 |
| Effective Green, g (s) | 15.0 | 21.3 | 21.3 | 17.0 | 23.3 | | 12.0 | 56.7 | 56.7 | 9.0 | 53.7 | 53.7 |
| Actuated g/C Ratio | 0.12 | 0.18 | 0.18 | 0.14 | 0.19 | | 0.10 | 0.47 | 0.47 | 0.08 | 0.45 | 0.45 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 1.0 | 1.0 | 1.0 | 3.0 | | 3.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lane Grp Cap (vph) | 225 | 337 | 286 | 255 | 330 | | 180 | 2450 | 763 | 135 | 1615 | 722 |
| v/s Ratio Prot | 0.12 | 0.07 | | c0.16 | c0.15 | | c0.11 | 0.35 | | c0.14 | c0.41 | |
| v/s Ratio Perm | | | 0.03 | | | | | | 0.11 | | | 0.05 |
| v/c Ratio | 0.98 | 0.40 | 0.16 | 1.12 | 0.79 | | 1.12 | 0.73 | 0.23 | 1.84 | 0.91 | 0.12 |
| Uniform Delay, d1 | 52.3 | 43.7 | 41.8 | 51.5 | 46.0 | | 54.0 | 25.5 | 18.7 | 55.5 | 31.0 | 19.4 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 53.1 | 0.3 | 0.1 | 91.7 | 12.1 | | 103.7 | 2.0 | 0.7 | 407.2 | 9.5 | 0.3 |
| Delay (s) | 105.4 | 44.0 | 41.9 | 143.2 | 58.2 | | 157.7 | 27.5 | 19.4 | 462.7 | 40.5 | 19.7 |
| Level of Service | F | D | D | F | Е | | F | С | В | F | D | В |
| Approach Delay (s) | | 68.4 | | | 97.2 | | | 38.0 | | | 95.6 | |
| Approach LOS | | E | | | F | | | D | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 68.3 | Н | CM 2000 | Level of S | Service | | Е | | | |
| HCM 2000 Volume to Capa | acity ratio | | 0.99 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | | um of lost | | | | 16.0 | | | |
| Intersection Capacity Utiliza | ation | | 97.2% | IC | CU Level of | of Service | | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

ATTACHMENT F

Long Range (2035) With Widening Conditions Intersection Operations Analysis Worksheets

| | ۶ | → | • | • | ← | • | 4 | † | / | > | ţ | 4 |
|--------------------------------|------------|----------|-------|-------|-----------|------------|---------|----------|----------|-------------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ¥ | † | 7 | 7 | f) | | J. | ተተተ | 7 | J. | ተተኈ | |
| Volume (vph) | 41 | 2 | 34 | 101 | 100 | 103 | 55 | 1189 | 281 | 93 | 1622 | 36 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1805 | 1900 | 1615 | 1805 | 1755 | | 1805 | 5187 | 1615 | 1805 | 5170 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1805 | 1900 | 1615 | 1805 | 1755 | | 1805 | 5187 | 1615 | 1805 | 5170 | |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 41 | 2 | 34 | 101 | 100 | 103 | 55 | 1189 | 281 | 93 | 1622 | 36 |
| RTOR Reduction (vph) | 0 | 0 | 31 | 0 | 38 | 0 | 0 | 0 | 119 | 0 | 1 | 0 |
| Lane Group Flow (vph) | 41 | 2 | 3 | 101 | 165 | 0 | 55 | 1189 | 162 | 93 | 1657 | 0 |
| Turn Type | Prot | NA | Perm | Prot | NA | | Prot | NA | Perm | Prot | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | | | 4 | | | | | | 6 | | | |
| Actuated Green, G (s) | 7.1 | 10.2 | 10.2 | 14.2 | 17.3 | | 8.0 | 69.0 | 69.0 | 10.6 | 71.6 | |
| Effective Green, g (s) | 7.1 | 10.2 | 10.2 | 14.2 | 17.3 | | 8.0 | 69.0 | 69.0 | 10.6 | 71.6 | |
| Actuated g/C Ratio | 0.06 | 0.08 | 0.08 | 0.12 | 0.14 | | 0.07 | 0.57 | 0.57 | 0.09 | 0.60 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 1.0 | 1.0 | 1.0 | 3.0 | | 3.0 | 1.0 | 1.0 | 1.0 | 1.0 | |
| Lane Grp Cap (vph) | 106 | 161 | 137 | 213 | 253 | | 120 | 2982 | 928 | 159 | 3084 | |
| v/s Ratio Prot | 0.02 | 0.00 | | c0.06 | c0.09 | | 0.03 | 0.23 | | c0.05 | c0.32 | |
| v/s Ratio Perm | | | 0.00 | | | | | | 0.10 | | | |
| v/c Ratio | 0.39 | 0.01 | 0.02 | 0.47 | 0.65 | | 0.46 | 0.40 | 0.17 | 0.58 | 0.54 | |
| Uniform Delay, d1 | 54.4 | 50.3 | 50.3 | 49.4 | 48.5 | | 53.9 | 14.1 | 12.0 | 52.6 | 14.4 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 2.3 | 0.0 | 0.0 | 0.6 | 5.9 | | 2.8 | 0.4 | 0.4 | 3.5 | 0.7 | |
| Delay (s) | 56.7 | 50.3 | 50.3 | 50.0 | 54.5 | | 56.7 | 14.5 | 12.5 | 56.1 | 15.0 | |
| Level of Service | Е | D | D | D | D | | Е | В | В | Е | В | |
| Approach Delay (s) | | 53.7 | | | 53.0 | | | 15.6 | | | 17.2 | |
| Approach LOS | | D | | | D | | | В | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 20.3 | Н | CM 2000 | Level of S | Service | | С | | | |
| HCM 2000 Volume to Capac | city ratio | | 0.57 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | | um of los | | | | 16.0 | | | |
| Intersection Capacity Utilizat | ion | | 63.7% | IC | CU Level | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| | ٠ | - | \rightarrow | • | ← | • | • | † | / | \ | ļ | 4 |
|-------------------------------|-------------|----------|---------------|-------|-------------|------------|---------|----------|------|----------|-------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | † | 7 | 7 | f) | | ň | ተተተ | 7 | Ţ | ↑ ↑₽ | |
| Volume (vph) | 220 | 135 | 182 | 285 | 105 | 230 | 202 | 1791 | 280 | 249 | 1476 | 132 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 0.90 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1805 | 1900 | 1615 | 1805 | 1704 | | 1805 | 5187 | 1615 | 1805 | 5123 | |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1805 | 1900 | 1615 | 1805 | 1704 | | 1805 | 5187 | 1615 | 1805 | 5123 | |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 220 | 135 | 182 | 285 | 105 | 230 | 202 | 1791 | 280 | 249 | 1476 | 132 |
| RTOR Reduction (vph) | 0 | 0 | 151 | 0 | 75 | 0 | 0 | 0 | 107 | 0 | 7 | 0 |
| Lane Group Flow (vph) | 220 | 135 | 31 | 285 | 260 | 0 | 202 | 1791 | 173 | 249 | 1601 | 0 |
| Turn Type | Prot | NA | Perm | Prot | NA | | Prot | NA | Perm | Prot | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | | | 4 | | | | | | 6 | | | |
| Actuated Green, G (s) | 15.0 | 20.3 | 20.3 | 18.0 | 23.3 | | 14.0 | 50.7 | 50.7 | 15.0 | 51.7 | |
| Effective Green, g (s) | 15.0 | 20.3 | 20.3 | 18.0 | 23.3 | | 14.0 | 50.7 | 50.7 | 15.0 | 51.7 | |
| Actuated g/C Ratio | 0.12 | 0.17 | 0.17 | 0.15 | 0.19 | | 0.12 | 0.42 | 0.42 | 0.12 | 0.43 | |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 1.0 | 1.0 | 1.0 | 3.0 | | 3.0 | 1.0 | 1.0 | 1.0 | 1.0 | |
| Lane Grp Cap (vph) | 225 | 321 | 273 | 270 | 330 | | 210 | 2191 | 682 | 225 | 2207 | |
| v/s Ratio Prot | 0.12 | 0.07 | | c0.16 | c0.15 | | 0.11 | c0.35 | | c0.14 | 0.31 | |
| v/s Ratio Perm | | | 0.02 | | | | | | 0.11 | | | |
| v/c Ratio | 0.98 | 0.42 | 0.11 | 1.06 | 0.79 | | 0.96 | 0.82 | 0.25 | 1.11 | 0.73 | |
| Uniform Delay, d1 | 52.3 | 44.6 | 42.2 | 51.0 | 46.0 | | 52.7 | 30.6 | 22.4 | 52.5 | 28.3 | |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 53.1 | 0.3 | 0.1 | 70.1 | 11.8 | | 51.0 | 3.5 | 0.9 | 91.5 | 2.1 | |
| Delay (s) | 105.4 | 44.9 | 42.3 | 121.1 | 57.8 | | 103.7 | 34.1 | 23.3 | 144.0 | 30.4 | |
| Level of Service | F | D | D | F | Е | | F | С | С | F | С | |
| Approach Delay (s) | | 68.8 | | | 86.9 | | | 39.0 | | | 45.6 | |
| Approach LOS | | Е | | | F | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 50.0 | Н | CM 2000 | Level of S | Service | | D | | | |
| HCM 2000 Volume to Capa | acity ratio | | 0.90 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | | um of lost | | | | 16.0 | | | |
| Intersection Capacity Utiliza | ation | | 93.6% | IC | CU Level of | of Service | | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

ATTACHMENT G

Long Range (2035) Without Widening Conditions Queuing Analysis Worksheets

| AM | Peak | Hour |
|----|------|------|

| | ۶ | → | • | • | • | • | 4 | † | / | > | ļ | 4 |
|-------------------------|------|----------|------|------|------|------|------|----------|----------|-------------|----------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | † | 7 | 7 | î» | | Ţ | ተተተ | 7 | 7 | ^ | 7 |
| Volume (vph) | 41 | 2 | 34 | 101 | 100 | 103 | 55 | 1189 | 281 | 93 | 1622 | 36 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 325 | | 100 | 0 | | 100 | 205 | | 220 | 250 | | 50 |
| Storage Lanes | 1 | | 1 | 1 | | 0 | 1 | | 1 | 1 | | 1 |
| Taper Length (ft) | 25 | | | 90 | | | 90 | | | 90 | | |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Link Speed (mph) | | 30 | | | 45 | | | 55 | | | 55 | |
| Link Distance (ft) | | 807 | | | 1355 | | | 2143 | | | 1222 | |
| Travel Time (s) | | 18.3 | | | 20.5 | | | 26.6 | | | 15.1 | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 41 | 2 | 34 | 101 | 100 | 103 | 55 | 1189 | 281 | 93 | 1622 | 36 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 41 | 2 | 34 | 101 | 203 | 0 | 55 | 1189 | 281 | 93 | 1622 | 36 |
| v/c Ratio | 0.34 | 0.01 | 0.14 | 0.47 | 0.73 | | 0.42 | 0.39 | 0.27 | 0.56 | 0.73 | 0.03 |
| Control Delay | 60.0 | 43.5 | 1.3 | 57.5 | 53.2 | | 62.3 | 15.9 | 2.7 | 64.5 | 21.8 | 0.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 60.0 | 43.5 | 1.3 | 57.5 | 53.2 | | 62.3 | 15.9 | 2.7 | 64.5 | 21.8 | 0.1 |
| Queue Length 50th (ft) | 31 | 1 | 0 | 77 | 120 | | 41 | 183 | 0 | 69 | 471 | 0 |
| Queue Length 95th (ft) | 67 | 9 | 0 | 132 | 191 | | 84 | 272 | 47 | 124 | #770 | 0 |
| Internal Link Dist (ft) | | 727 | | | 1275 | | | 2063 | | | 1142 | |
| Turn Bay Length (ft) | 325 | | 100 | | | | 205 | | 220 | 250 | | 50 |
| Base Capacity (vph) | 210 | 506 | 490 | 266 | 528 | | 165 | 3030 | 1060 | 210 | 2236 | 1032 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.20 | 0.00 | 0.07 | 0.38 | 0.38 | | 0.33 | 0.39 | 0.27 | 0.44 | 0.73 | 0.03 |

Intersection Summary

Area Type: Other

Queue shown is maximum after two cycles.

^{# 95}th percentile volume exceeds capacity, queue may be longer.

| Trineritary / tri (i | - , | | , – (| , | | | | | | | | |
|-------------------------|-------|----------|---------------|-------|----------|------|----------|----------|----------|-------|----------|------|
| | • | → | \rightarrow | • | ← | • | 1 | † | / | - | ţ | 4 |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | Ť | | 7 | , j | ĵ. | | * | ^ | 7 | ¥ | † | 7 |
| Volume (vph) | 220 | 135 | 182 | 285 | 105 | 230 | 202 | 1791 | 280 | 249 | 1476 | 132 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 325 | | 100 | 0 | | 100 | 205 | | 220 | 250 | | 50 |
| Storage Lanes | 1 | | 1 | 1 | | 0 | 1 | | 1 | 1 | | 1 |
| Taper Length (ft) | 25 | | | 90 | | | 90 | | | 90 | | |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Link Speed (mph) | | 30 | | | 45 | | | 55 | | | 55 | |
| Link Distance (ft) | | 807 | | | 1355 | | | 2143 | | | 1222 | |
| Travel Time (s) | | 18.3 | | | 20.5 | | | 26.6 | | | 15.1 | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 220 | 135 | 182 | 285 | 105 | 230 | 202 | 1791 | 280 | 249 | 1476 | 132 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 220 | 135 | 182 | 285 | 335 | 0 | 202 | 1791 | 280 | 249 | 1476 | 132 |
| v/c Ratio | 1.05 | 0.40 | 0.42 | 1.19 | 0.83 | | 1.22 | 0.79 | 0.34 | 1.19 | 0.88 | 0.17 |
| Control Delay | 126.4 | 45.4 | 8.3 | 163.2 | 49.9 | | 188.4 | 33.1 | 9.3 | 167.0 | 37.8 | 9.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 126.4 | 45.4 | 8.3 | 163.2 | 49.9 | | 188.4 | 33.1 | 9.3 | 167.0 | 37.8 | 9.7 |
| Queue Length 50th (ft) | ~185 | 93 | 0 | ~265 | 186 | | ~192 | 427 | 39 | ~232 | 533 | 21 |
| Queue Length 95th (ft) | #345 | 141 | 57 | #440 | 270 | | #345 | #600 | 115 | #398 | #798 | 66 |
| Internal Link Dist (ft) | | 727 | | | 1275 | | | 2063 | | | 1142 | |
| Turn Bay Length (ft) | 325 | | 100 | | | | 205 | | 220 | 250 | | 50 |
| Base Capacity (vph) | 210 | 506 | 564 | 240 | 548 | | 165 | 2277 | 817 | 210 | 1674 | 793 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | | | | | | |

Intersection Summary

Reduced v/c Ratio

Area Type:

1.05

0.27

0.32

1.19

0.61

1.22

0.79

0.34

1.19

0.88

0.17

Queue shown is maximum after two cycles.

Other Volume exceeds capacity, queue is theoretically infinite. Queue shown is maximum after two cycles.

⁹⁵th percentile volume exceeds capacity, queue may be longer.

ATTACHMENT H

Long Range (2035) With Widening Conditions Queuing Analysis Worksheets

| | | AM Pea | ık Hour |
|-----|----------|-----------------|---------|
| / | / | ţ | 1 |
| NBR | SBL | SBT | SBR |
| 7 | , J | ተተ _ጉ | |

| | • | → | * | • | • | • | 1 | Ť | | - | ¥ | 4 |
|-------------------------|------|----------|------|------|------|------|------|------|------|------|------------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ħ | † | 7 | ħ | î, | | 7 | ተተተ | 7 | ħ | ↑ ↑ | |
| Volume (vph) | 41 | 2 | 34 | 101 | 100 | 103 | 55 | 1189 | 281 | 93 | 1622 | 36 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 325 | | 100 | 0 | | 100 | 205 | | 220 | 250 | | 50 |
| Storage Lanes | 1 | | 1 | 1 | | 0 | 1 | | 1 | 1 | | 0 |
| Taper Length (ft) | 25 | | | 90 | | | 90 | | | 90 | | |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Link Speed (mph) | | 30 | | | 45 | | | 55 | | | 55 | |
| Link Distance (ft) | | 807 | | | 1355 | | | 2143 | | | 1222 | |
| Travel Time (s) | | 18.3 | | | 20.5 | | | 26.6 | | | 15.1 | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 41 | 2 | 34 | 101 | 100 | 103 | 55 | 1189 | 281 | 93 | 1622 | 36 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 41 | 2 | 34 | 101 | 203 | 0 | 55 | 1189 | 281 | 93 | 1658 | 0 |
| v/c Ratio | 0.34 | 0.01 | 0.14 | 0.47 | 0.73 | | 0.40 | 0.39 | 0.26 | 0.63 | 0.52 | |
| Control Delay | 60.0 | 43.5 | 1.3 | 57.6 | 53.0 | | 60.4 | 15.2 | 2.7 | 71.2 | 16.5 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 60.0 | 43.5 | 1.3 | 57.6 | 53.0 | | 60.4 | 15.2 | 2.7 | 71.2 | 16.5 | |
| Queue Length 50th (ft) | 31 | 1 | 0 | 77 | 120 | | 41 | 175 | 0 | 71 | 270 | |
| Queue Length 95th (ft) | 67 | 9 | 0 | 132 | 190 | | 82 | 272 | 47 | 123 | 412 | |
| Internal Link Dist (ft) | | 727 | | | 1275 | | | 2063 | | | 1142 | |
| Turn Bay Length (ft) | 325 | | 100 | | | | 205 | | 220 | 250 | | |
| Base Capacity (vph) | 225 | 506 | 490 | 290 | 543 | | 210 | 3085 | 1074 | 225 | 3189 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.18 | 0.00 | 0.07 | 0.35 | 0.37 | | 0.26 | 0.39 | 0.26 | 0.41 | 0.52 | |
| Intersection Summary | | | | | | | | | | | | |

Area Type:

Other

| 1. Monterey Av. (I | io) a Di | N IVEII | y Di. (| <u> </u> | | | | | | | 1 101 1 00 | art 110ui |
|-------------------------|----------|----------|---------|----------|------|------|-------|----------|------|----------|-----------------|-----------|
| | • | → | * | • | + | • | • | † | ~ | \ | ↓ | -√ |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | † | 7 | Ţ | ĵ. | | ň | ^ | 7 | 7 | ተተ _ጉ | |
| Volume (vph) | 220 | 135 | 182 | 285 | 105 | 230 | 202 | 1791 | 280 | 249 | 1476 | 132 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 325 | | 100 | 0 | | 100 | 205 | | 220 | 250 | | 50 |
| Storage Lanes | 1 | | 1 | 1 | | 0 | 1 | | 1 | 1 | | 0 |
| Taper Length (ft) | 25 | | | 90 | | | 90 | | | 90 | | |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Link Speed (mph) | | 30 | | | 45 | | | 55 | | | 55 | |
| Link Distance (ft) | | 807 | | | 1355 | | | 2143 | | | 1222 | |
| Travel Time (s) | | 18.3 | | | 20.5 | | | 26.6 | | | 15.1 | |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 220 | 135 | 182 | 285 | 105 | 230 | 202 | 1791 | 280 | 249 | 1476 | 132 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 220 | 135 | 182 | 285 | 335 | 0 | 202 | 1791 | 280 | 249 | 1608 | 0 |
| v/c Ratio | 0.98 | 0.42 | 0.43 | 1.06 | 0.83 | | 0.96 | 0.82 | 0.35 | 1.11 | 0.73 | |
| Control Delay | 107.3 | 46.8 | 8.6 | 119.2 | 49.5 | | 106.1 | 35.5 | 10.4 | 139.8 | 31.6 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 107.3 | 46.8 | 8.6 | 119.2 | 49.5 | | 106.1 | 35.5 | 10.4 | 139.8 | 31.6 | |
| Queue Length 50th (ft) | 172 | 94 | 0 | ~241 | 185 | | 158 | 441 | 44 | ~220 | 368 | |
| Queue Length 95th (ft) | #332 | 143 | 57 | #415 | 269 | | #309 | #626 | 124 | #386 | 489 | |
| Internal Link Dist (ft) | | 727 | | | 1275 | | | 2063 | | | 1142 | |
| Turn Bay Length (ft) | 325 | | 100 | | | | 205 | | 220 | 250 | | |
| Base Capacity (vph) | 225 | 506 | 564 | 270 | 562 | | 210 | 2190 | 789 | 225 | 2214 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | |
| | | | | | | | | | | | | |

Intersection Summary

Reduced v/c Ratio

Area Type: Other

0.98

0.27

0.32

1.06

0.60

0.96

0.82

0.35

1.11

0.73

Queue shown is maximum after two cycles.

Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.

^{# 95}th percentile volume exceeds capacity, queue may be longer.

ATTACHMENT I

Opening Year 2014 Without Project Intersection Operations Analysis Worksheets

| | • | • | ₹I | † | / | > | ↓ |
|--------------------------------|------------|------|-------|----------|------------|-------------|----------|
| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT |
| Lane Configurations | ሻ | 7 | Ð | ተተተ | 7 | ሻ | ^ |
| Volume (vph) | 80 | 17 | 0 | 732 | 58 | 19 | 1189 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 5.0 | 5.0 | 4.0 | 5.0 |
| Lane Util. Factor | 1.00 | 1.00 | | 0.91 | 1.00 | 1.00 | 0.95 |
| Frt | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 1.00 |
| Flt Protected | 0.95 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 1805 | 1615 | | 5187 | 1615 | 1805 | 3610 |
| Flt Permitted | 0.95 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (perm) | 1805 | 1615 | | 5187 | 1615 | 1805 | 3610 |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Adj. Flow (vph) | 90 | 19 | 0 | 822 | 65 | 21 | 1336 |
| RTOR Reduction (vph) | 0 | 18 | 0 | 0 | 13 | 0 | 0 |
| Lane Group Flow (vph) | 90 | 1 | 0 | 822 | 52 | 21 | 1336 |
| Turn Type | NA | Perm | Prot | NA | Perm | Prot | NA |
| Protected Phases | 3 | | 1 | 6 | | 5 | 2 |
| Permitted Phases | | 3 | | | 6 | | |
| Actuated Green, G (s) | 9.4 | 9.4 | | 95.1 | 95.1 | 2.5 | 101.6 |
| Effective Green, g (s) | 9.4 | 9.4 | | 95.1 | 95.1 | 2.5 | 101.6 |
| Actuated g/C Ratio | 0.08 | 0.08 | | 0.79 | 0.79 | 0.02 | 0.85 |
| Clearance Time (s) | 4.0 | 4.0 | | 5.0 | 5.0 | 4.0 | 5.0 |
| Vehicle Extension (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | 1.0 |
| Lane Grp Cap (vph) | 141 | 126 | | 4110 | 1279 | 37 | 3056 |
| v/s Ratio Prot | c0.05 | | | 0.16 | | 0.01 | c0.37 |
| v/s Ratio Perm | | 0.00 | | | 0.03 | | |
| v/c Ratio | 0.64 | 0.01 | | 0.20 | 0.04 | 0.57 | 0.44 |
| Uniform Delay, d1 | 53.7 | 51.0 | | 3.1 | 2.7 | 58.2 | 2.2 |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 6.8 | 0.0 | | 0.1 | 0.1 | 11.3 | 0.5 |
| Delay (s) | 60.4 | 51.0 | | 3.2 | 2.7 | 69.6 | 2.7 |
| Level of Service | Е | D | | Α | Α | Ε | Α |
| Approach Delay (s) | 58.8 | | | 3.1 | | | 3.7 |
| Approach LOS | Е | | | Α | | | Α |
| Intersection Summary | | | | | | | |
| HCM 2000 Control Delay | | | 6.1 | H | CM 2000 | Level of | Service |
| HCM 2000 Volume to Capac | city ratio | | 0.47 | | | | |
| Actuated Cycle Length (s) | | | 120.0 | S | um of lost | time (s) | |
| Intersection Capacity Utilizat | ion | | 44.8% | | CU Level c | | |
| Analysis Period (min) | | | 15 | | | | |
| c Critical Lane Group | | | | | | | |

| | • | • | ∳ I | † | / | > | ↓ | | | |
|--------------------------------|------------|------|------------|----------|-----------|-------------|----------|------|---|--|
| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT | | | |
| Lane Configurations | ሻ | 7 | Ð | ተተተ | 7 | ሻ | ^ | | | |
| Volume (vph) | 217 | 52 | 0 | 1366 | 138 | 46 | 959 | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | | | |
| Total Lost time (s) | 4.0 | 4.0 | | 5.0 | 5.0 | 4.0 | 5.0 | | | |
| Lane Util. Factor | 1.00 | 1.00 | | 0.91 | 1.00 | 1.00 | 0.95 | | | |
| Frt | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 1.00 | | | |
| Flt Protected | 0.95 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 | | | |
| Satd. Flow (prot) | 1805 | 1615 | | 5187 | 1615 | 1805 | 3610 | | | |
| Flt Permitted | 0.95 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 | | | |
| Satd. Flow (perm) | 1805 | 1615 | | 5187 | 1615 | 1805 | 3610 | | | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | | | |
| Adj. Flow (vph) | 228 | 55 | 0 | 1438 | 145 | 48 | 1009 | | | |
| RTOR Reduction (vph) | 0 | 47 | 0 | 0 | 43 | 0 | 0 | | | |
| Lane Group Flow (vph) | 228 | 8 | 0 | 1438 | 102 | 48 | 1009 | | | |
| Turn Type | NA | Perm | Prot | NA | Perm | Prot | NA | | | |
| Protected Phases | 3 | | 1 | 6 | | 5 | 2 | | | |
| Permitted Phases | | 3 | | | 6 | | | | | |
| Actuated Green, G (s) | 16.7 | 16.7 | | 84.7 | 84.7 | 5.6 | 94.3 | | | |
| Effective Green, g (s) | 16.7 | 16.7 | | 84.7 | 84.7 | 5.6 | 94.3 | | | |
| Actuated g/C Ratio | 0.14 | 0.14 | | 0.71 | 0.71 | 0.05 | 0.79 | | | |
| Clearance Time (s) | 4.0 | 4.0 | | 5.0 | 5.0 | 4.0 | 5.0 | | | |
| Vehicle Extension (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | 1.0 | | | |
| Lane Grp Cap (vph) | 251 | 224 | | 3661 | 1139 | 84 | 2836 | | | |
| v/s Ratio Prot | c0.13 | | | c0.28 | | c0.03 | 0.28 | | | |
| v/s Ratio Perm | | 0.00 | | | 0.06 | | | | | |
| v/c Ratio | 0.91 | 0.03 | | 0.39 | 0.09 | 0.57 | 0.36 | | | |
| Uniform Delay, d1 | 50.9 | 44.7 | | 7.2 | 5.5 | 56.0 | 3.8 | | | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | 32.6 | 0.0 | | 0.3 | 0.2 | 5.7 | 0.4 | | | |
| Delay (s) | 83.5 | 44.7 | | 7.5 | 5.7 | 61.7 | 4.2 | | | |
| Level of Service | F | D | | A | Α | E | Α | | | |
| Approach Delay (s) | 75.9 | | | 7.3 | | | 6.8 | | | |
| Approach LOS | Е | | | А | | | Α | | | |
| Intersection Summary | | | | | | | | | | |
| HCM 2000 Control Delay | | | 13.8 | Н | CM 2000 | Level of S | Service | E | 3 | |
| HCM 2000 Volume to Capac | city ratio | | 0.48 | | | | | | | |
| Actuated Cycle Length (s) | _ | | 120.0 | S | um of los | t time (s) | | 13.0 |) | |
| Intersection Capacity Utilizat | tion | | 53.4% | | | of Service | | A | | |
| Analysis Period (min) | | | 15 | | | | | | | |
| c Critical Lane Group | | | | | | | | | | |

ATTACHMENT J

Opening Year 2014 With Project Intersection Operations Analysis Worksheets

| | • | • | ∳ I | † | ~ | - | ļ | | |
|-------------------------------|-------------|------|------------|----------|-----------|------------|----------|------|--|
| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT | | |
| Lane Configurations | * | 7 | Ð | ^ | 7 | ሻ | ተተተ | | |
| Volume (vph) | 80 | 17 | 0 | 732 | 58 | 19 | 1189 | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | | |
| Total Lost time (s) | 4.0 | 4.0 | | 5.0 | 5.0 | 4.0 | 5.0 | | |
| Lane Util. Factor | 1.00 | 1.00 | | 0.91 | 1.00 | 1.00 | 0.91 | | |
| Frt | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 1.00 | | |
| Flt Protected | 0.95 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 | | |
| Satd. Flow (prot) | 1805 | 1615 | | 5187 | 1615 | 1805 | 5187 | | |
| Flt Permitted | 0.95 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 | | |
| Satd. Flow (perm) | 1805 | 1615 | | 5187 | 1615 | 1805 | 5187 | | |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | | |
| Adj. Flow (vph) | 90 | 19 | 0 | 822 | 65 | 21 | 1336 | | |
| RTOR Reduction (vph) | 0 | 18 | 0 | 0 | 13 | 0 | 0 | | |
| Lane Group Flow (vph) | 90 | 1 | 0 | 822 | 52 | 21 | 1336 | | |
| Turn Type | NA | Perm | Prot | NA | Perm | Prot | NA | | |
| Protected Phases | 3 | | 1 | 6 | | 5 | 2 | | |
| Permitted Phases | | 3 | | | 6 | | | | |
| Actuated Green, G (s) | 9.4 | 9.4 | | 95.1 | 95.1 | 2.5 | 101.6 | | |
| Effective Green, g (s) | 9.4 | 9.4 | | 95.1 | 95.1 | 2.5 | 101.6 | | |
| Actuated g/C Ratio | 0.08 | 0.08 | | 0.79 | 0.79 | 0.02 | 0.85 | | |
| Clearance Time (s) | 4.0 | 4.0 | | 5.0 | 5.0 | 4.0 | 5.0 | | |
| Vehicle Extension (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | 1.0 | | |
| Lane Grp Cap (vph) | 141 | 126 | | 4110 | 1279 | 37 | 4391 | | |
| v/s Ratio Prot | c0.05 | | | 0.16 | | c0.01 | c0.26 | | |
| v/s Ratio Perm | | 0.00 | | | 0.03 | | | | |
| v/c Ratio | 0.64 | 0.01 | | 0.20 | 0.04 | 0.57 | 0.30 | | |
| Uniform Delay, d1 | 53.7 | 51.0 | | 3.1 | 2.7 | 58.2 | 1.9 | | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | | |
| Incremental Delay, d2 | 6.8 | 0.0 | | 0.1 | 0.1 | 11.3 | 0.2 | | |
| Delay (s) | 60.4 | 51.0 | | 3.2 | 2.7 | 69.6 | 2.1 | | |
| Level of Service | Е | D | | Α | Α | Ε | Α | | |
| Approach Delay (s) | 58.8 | | | 3.1 | | | 3.1 | | |
| Approach LOS | Е | | | А | | | Α | | |
| Intersection Summary | | | | | | | | | |
| HCM 2000 Control Delay | | | 5.7 | Н | CM 2000 | Level of | Service | А | |
| HCM 2000 Volume to Capa | icity ratio | | 0.35 | | | | | | |
| Actuated Cycle Length (s) | • | | 120.0 | S | um of los | t time (s) | | 13.0 | |
| Intersection Capacity Utiliza | ation | | 34.9% | | CU Level | |) | А | |
| Analysis Period (min) | | | 15 | | | | | | |
| c Critical Lane Group | | | | | | | | | |

| | • | • | ₹I | † | / | > | ļ | |
|--------------------------------|------------|------|-------|----------|-------------|-------------|----------|--|
| Movement | WBL | WBR | NBU | NBT | NBR | SBL | SBT | |
| Lane Configurations | * | 7 | Ð | ተተተ | 7 | ሻ | ^ | |
| Volume (vph) | 217 | 52 | 0 | 1366 | 138 | 46 | 959 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Total Lost time (s) | 4.0 | 4.0 | | 5.0 | 5.0 | 4.0 | 5.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 0.91 | 1.00 | 1.00 | 0.91 | |
| Frt | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 1.00 | |
| Flt Protected | 0.95 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1805 | 1615 | | 5187 | 1615 | 1805 | 5187 | |
| Flt Permitted | 0.95 | 1.00 | | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (perm) | 1805 | 1615 | | 5187 | 1615 | 1805 | 5187 | |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | |
| Adj. Flow (vph) | 228 | 55 | 0 | 1438 | 145 | 48 | 1009 | |
| RTOR Reduction (vph) | 0 | 47 | 0 | 0 | 43 | 0 | 0 | |
| Lane Group Flow (vph) | 228 | 8 | 0 | 1438 | 102 | 48 | 1009 | |
| Turn Type | NA | Perm | Prot | NA | Perm | Prot | NA | |
| Protected Phases | 3 | | 1 | 6 | | 5 | 2 | |
| Permitted Phases | | 3 | | | 6 | | | |
| Actuated Green, G (s) | 16.7 | 16.7 | | 84.7 | 84.7 | 5.6 | 94.3 | |
| Effective Green, g (s) | 16.7 | 16.7 | | 84.7 | 84.7 | 5.6 | 94.3 | |
| Actuated g/C Ratio | 0.14 | 0.14 | | 0.71 | 0.71 | 0.05 | 0.79 | |
| Clearance Time (s) | 4.0 | 4.0 | | 5.0 | 5.0 | 4.0 | 5.0 | |
| Vehicle Extension (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | 1.0 | |
| Lane Grp Cap (vph) | 251 | 224 | | 3661 | 1139 | 84 | 4076 | |
| v/s Ratio Prot | c0.13 | | | c0.28 | | c0.03 | 0.19 | |
| v/s Ratio Perm | | 0.00 | | | 0.06 | | | |
| v/c Ratio | 0.91 | 0.03 | | 0.39 | 0.09 | 0.57 | 0.25 | |
| Uniform Delay, d1 | 50.9 | 44.7 | | 7.2 | 5.5 | 56.0 | 3.4 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 32.6 | 0.0 | | 0.3 | 0.2 | 5.7 | 0.1 | |
| Delay (s) | 83.5 | 44.7 | | 7.5 | 5.7 | 61.7 | 3.6 | |
| Level of Service | F | D | | Α | А | Е | Α | |
| Approach Delay (s) | 75.9 | | | 7.3 | | | 6.2 | |
| Approach LOS | E | | | Α | | | Α | |
| Intersection Summary | | | | | | | | |
| HCM 2000 Control Delay | | | 13.6 | Н | CM 2000 | Level of S | Service | |
| HCM 2000 Volume to Capac | city ratio | | 0.48 | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | | um of lost | | | |
| Intersection Capacity Utilizat | tion | | 53.4% | IC | CU Level of | of Service | | |
| Analysis Period (min) | | | 15 | | | | | |
| c Critical Lane Group | | | | | | | | |